Effects of Thermal Radiation and Heat Source/Sink on Powell-Eyring Nanofluid with Variable Thickness

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Abstract

A steady boundary layer flow of Powell- Eyring nanofluid past a stretching sheet with variable thickness in the presence of thermal radiation and heat source/sink is studied numerically. The model is used for the nanofluid incorporates the effects of Brownian motion and thermophoresis. The suitable transformations are applied to convert the governing partial differential equations into a set of nonlinear coupled ordinary differential equations. Runge-Kutta-based shooting technique is employed to yield the numerical solutions for the model. The obtained results for the velocity, temperature and concentration are analyzed graphically for several physical parameters. It is found that an increment in wall thickness parameter results in decrease of velocity, temperature and concentration profiles. Further, in tabular form the numerical values are given for the local skin friction coefficient, local Nusselt number and Sherwood number. A remarkable agreement is noticed by comparing the present results with the results reported in the literature as a special case.

Keywords: Thermal Radiation, Powell – Eyring fluid, Heat Source/Sink, MHD.
1. INTRODUCTION

Viscous boundary layer flow due to a stretching/shrinking sheet is of significant importance due to its vast applications. Aerodynamic extrusion of plastic sheets, glass fiber production, paper production, heat treated materials travelling between a feed roll and a wind-up roll, cooling of an infinite metallic plate in a cooling bath and manufacturing of polymeric sheets are some examples for practical applications of non-Newtonian fluid flow over a stretching/shrinking surface. The quality of the final product depends on the rate of heat transfer at the stretching surface. This stretching/shrinking may not necessarily be linear. It may be quadratic, power-law, exponential and so on. Bilal Asharf et.al. [1] studied the three dimensional boundary layer flow of Eyring-Powell nanofluid by convectively heated exponentially stretching sheet. Hayat et.al. [2] investigated the axisymmetric Powell-Eyring fluid flow with convective boundary condition. Javed et.al. [3] analyzed the boundary layer flow of an Eyring -Powell non-Newtonian fluid over a stretching sheet. Hayat et.al. [4] studied the effect of MHD boundary layer flow of Powell-Eyring nanofluid over a non-linear stretching sheet with variable thickness. Nazar et.al. [5] investigated the mixed convection boundary layer flow an isothermal horizontal circular cylinder embedded in a porous medium filled with a nanofluid for both cases of a heated and cooled cylinder.

Solar energy is probably the most suitable source of renewable energy that can meet the current energy requirements. The energy obtained from nature in the form of solar radiations can be directly transformed into heat and electricity. The idea of using small particles to collect solar energy was first investigated by Hunt [6] in the 1970s. Researchers concluded that with the addition of nanoparticles in the base fluids, heat transfer and the solar collection processes can be improved. Masuda et al. [7] discussed the alteration of thermal conductivity and viscosity by dispersing ultra-fine particles in the liquid. Choi and Eastman [8] were the first to introduce the terminology of nanofluids when they experimentally discovered an effective way of controlling heat transfer rate using nanoparticles. Buongiorno [9] developed the nonhomogeneous equilibrium mathematical model for convective transport of nanofluids. He concluded that Brownian motion and thermophoretic diffusion of nanoparticles are the most important mechanisms for the abnormal convective heat transfer enhancement. The relevant processes are briefly described in [10–12]. Investigations in the nanofluid flows have received remarkable popularity in research community in last couple of decades primarily due to their variety of applications in power generation, in transportation where nanofluid may be utilized in vehicles as coolant, shock absorber, fuel additives etc., in cooling and heating problems which may involve the use of nanofluids for cooling of microchips in computer processors, in improving performance efficiency of refrigerant/air-conditioners etc. and in biomedical applications in which magnetic nanoparticles may be used in medicine,
cancer therapy and tumor analysis. Recently the researchers have proposed the idea of using solar collector based nanofluids for optimal utilization of solar energy radiation [13, 14]. Buongiorno and Hu [15] discussed the heat transfer enhancement via nanoparticles for nuclear reactor application. Huminic and Huminic [16] showed that use of nanofluids in heat exchangers has advantage in the energy efficiency and it leads to better system performance. Ramzan et al. [17] discussed effects radiation and MHD on Powell-Eyring nanofluid over a stretching cylinder with chemical reaction. Ullah et al. [18] studied theoretically the influence of thermal radiation and MHD on natural convective flow of casson nanofluid over a non linearly stretching sheet. Mustafa et al. [19] Runge-Kutta fourth –fifth order method with shooting technique to explore the steady boundary layer flow of nanofluid past a vertical plate with nonlinear radiation. Numerical solution for steady boundary layer flow of dusty fluid over a radiating stretching surface embedded in a thermally stratified porous medium in the presence of uniform heat source was studied by Gireesha et al. [20]. Recently, Ramzan et al. [21] analyzed the radiative Jeffery nanofluid with convective heat and mass conditions.

To the best of the author’s knowledge, there seems no existing document about steady boundary layer flow of Powell-Eyring nanofluid past a stretching sheet with variable thickness in the presence of thermal radiation and heat source/sink. Hence the aim of the present investigation is to examine the steady boundary layer flow of Powell-Eyring nanofluid past a stretching sheet with variable thickness in the presence of thermal radiation and heat source/sink.

2. MATHEMATICAL FORMULATION:

Radiative powell-Eyring nanofluid over an impermeable nonlinear heated stretching sheet with variable thickness is considered. An incompressible fluid is selected electrically conducting. A non-uniform magnetic field \( B(x) = B_0(x+b)^{\frac{n-1}{2}} \) is imposed transverse to the stretching sheet. Magnetic Reynolds number is chosen small. Induced magnetic and electric fields are not accounted. Brownian and thermophoresis in the nanofluid are considered. Newly developed condition for mass flux is imposed. The fluid formation is such that the x-axis is presumed along the sheet while y-axis is transverse to it. The temperature of the sheet is different from that of the ambient medium. The fluid viscosity is assumed to vary with the temperature while the other fluid properties are assumed constant.

In order to get the effect of temperature difference between the sheet and the ambient fluid we consider temperature dependent heat source/sink in the flow region. In this study we consider that the volumetric rate of heat generation, denoted by \( q^n = Q_0(T - T_\infty) \) for \( T \geq T_\infty \) and equal to zero for \( T \leq T_\infty \) where \( Q_0(>0) \) is the heat
generation $Q_0(<0)$ is the heat absorption constant (Vajravelu and Hadjinicolau [22]).

The stretching surface has the nonlinear velocity $U_w = U_0(x + b)^n$ where $U_0$ is the reference velocity and $b$ is the dimensional constant. Further it is assumed that sheet at $y = A(x + b)^{1-n}$ is not flat (where $n$ is the velocity power index and $A$ is assumed very small so that the sheet retain adequately thin). We also noticed that for $n=1$ the problem reduces to a flat sheet. The governing expressions for considered flow are given by:

\[
\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0
\]  

(1)

\[
\frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \left( v + \frac{1}{\rho \beta d} \right) \frac{\partial^2 u}{\partial y^2} - \frac{1}{2 \rho \beta d^3} \left( \frac{\partial u}{\partial y} \right)^2 \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B^2(x)}{\rho} u
\]  

(2)

\[
\frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha_{nf} \frac{\partial^2 T}{\partial y^2} + \frac{T}{T_c} \left( \frac{T}{T_c} \right)^{\frac{1}{2}} \frac{\partial q}{\partial y} + \frac{q_0}{(\rho c)_f} (T - T_c)
\]  

(3)

\[
\frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = D_B \frac{\partial^2 C}{\partial y^2} + D_T \left( \frac{\partial^2 T}{\partial y^2} \right)
\]  

(4)

With boundary conditions

\[
u = U_w(x) = U_0(x + b)^n, \quad v = 0, \quad T = T_w, \quad C = C_w \quad \text{at} \quad y = A(x + b)^{1-n}
\]

(5)

\[
u \to 0, \quad v \to 0, \quad T \to T_c, \quad C \to C_c \quad \text{as} \quad y \to \infty
\]

(6)

Here $u$ and $v$ are the corresponding velocity components parallel to $x$- and $y$-directions respectively, $\mu$ the dynamic viscosity, $v = \frac{\mu}{\rho}$ designates the kinematic viscosity, $\rho$ the fluid density, $d$ and $\beta$ are the material liquid parameters of Powell-Eyring model, $k$ the thermal conductivity, $\alpha_{nf} = \frac{k}{(\rho c)_f}$ the thermal diffusivity of liquid, $\tau$ the ratio of the heat capacity of liquid of the nanoparticles material to the effective heat capacity of the base fluid, $D_B$ indicates the Brownian diffusion coefficient, $D_T$ represents the thermophoretic diffusion, $Q_0[J s^{-1} m^{-3} K^{-1}]$ is the dimensional heat generation ($Q_0 > 0$) or absorption ($Q_0 < 0$) coefficient, $T$ the temperature of the fluid,
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The nanoparticles concentration, $T_w$ and $T_\infty$ are the sheet and ambient fluid temperatures and $C_w$ the ambient fluid nanoparticles concentration.

![Figure 1: Physical model and coordinate system](image)

Using the Rosseland approximations, the radiative heat flux is given by

$$q_r = -\frac{4\sigma^* \partial T^4}{3K^* \partial z} \quad (7)$$

Where, $\sigma^*$ and $K^*$ are, respectively, the Stephan – Boltzman constant and the mean absorption coefficient. Assume that the temperature differences within the flow are small such that $T^4$ in a Taylor series about $T_\infty$ and neglecting higher order terms. We get

$$T^4 \cong 4T_wT - 3T_\infty^4 \quad (8)$$

Substituting eq.’s (7) and (8) in eq. (3). We have

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \left( \alpha_f + \frac{16T_w\sigma^*}{3K^*(\rho \alpha)} \right) \frac{\partial^2 T}{\partial y^2} + \tau \left( D_g \frac{\partial T}{\partial y} \frac{\partial C}{\partial y} + \frac{D_T}{T_\infty} \left( \frac{\partial T}{\partial y} \right)^2 \right) + \frac{q_0}{(\rho \alpha)}(T - T_\infty) \quad (9)$$

Transformations are expressed as follows:
Incompressibility condition is satisfied identically and Eqs.(2), (4)-(6) and (9) take the following forms:

\[(1 + N)F'' + FF'' - \left( \frac{2n}{n+1} \right) F'' - N\left( \frac{n+1}{2} \right) \alpha F'' - \left( \frac{2}{n+1} \right) MF' = 0\]  

\[\left( \frac{1 + Nr}{Pr} \right) \Theta + F\Theta' + N'\theta' + N\theta' = 0\]

\[\Phi' + \text{Pr} LeF'\Phi' + \left( \frac{N_t}{N_b} \right) \Theta' = 0\]

\[F(\alpha) = \alpha \left( \frac{1-n}{1+n} \right), \quad F'(\alpha) = 1, \quad \Theta(\alpha) = 1, \quad \Phi(\alpha) = 1\]

\[F'(\infty) \rightarrow 0, \quad \Theta'(\infty) \rightarrow 0, \quad \Phi(\infty) \rightarrow 0\]  

In the above expressions primes designate differentiation with respect to \( \eta \), where \( \alpha = A \sqrt{\left( \frac{n+1}{2} \right) \frac{U_o}{\nu}} \) is the wall thickness parameter and \( \eta = A \sqrt{\left( \frac{n+1}{2} \right) \frac{U_o}{\nu}} \) shows the plate surface. Upon using

\[F(\eta) = f(\eta - \alpha), \quad \Theta(\eta) = \theta(\eta - \alpha), \quad \Phi(\eta) = \phi(\eta - \alpha) = \phi(\xi)\]

Eqs.(11)-(15) yield (See fig.1).

\[(1 + N)F'' + FF'' - \left( \frac{2n}{n+1} \right) F'' - N\left( \frac{n+1}{2} \right) \alpha F'' - \left( \frac{2}{n+1} \right) MF' = 0\]

\[\frac{1 + Nr}{Pr} \theta' + f\theta' + N\theta' + N\theta' + Q\theta = 0\]

\[\phi'' + \text{Pr} Le\phi' + \left( \frac{N_t}{N_b} \right) \theta'' = 0\]

\[f(0) = \alpha \left( \frac{1-n}{1+n} \right), \quad f'(0) = 1, \quad \theta(0) = 1, \quad \phi(0) = 1\]

\[f'(\infty) = 0, \quad \theta(\infty) = 0, \quad \phi(\infty) = 0\]
where $N$ and $\lambda$ are the fluid parameters, $M$ represents the magnetic parameter, $Nb$ the Brownian motion parameter, $Pr$ the Prandtl number, $Nt$ the thermophoresis parameter, $Le$ presents Lewis number, $Nr$ the radiation parameter, $Q$ the heat source/sink parameter and prime indicates differentiation with respect to $\xi$. The non-dimensional parameters are

$$N = \frac{1}{d\beta \mu}, \quad \lambda = \frac{U_0^3}{4d^2v}(x+b)^{n-1}, \quad M = \frac{\sigma B_i^2}{\rho U_0}, \quad Pr = \frac{v}{\alpha_f}, \quad Nb = \frac{D_B(C_w-C_o)}{v}$$

$$Nt = \frac{D_1(T_w-T_o)}{v T_w}, \quad Le = \frac{\alpha_f}{D_B}, \quad Nr = \frac{16\sigma^* T_w^3}{k K_*}, \quad Q = \frac{Q_0}{(\rho c)_j U_0}$$

Surface drag coefficient and surface heat transfer are expressed as follows:

$$C_f = \frac{2\tau_w}{\rho_f U_w^2}, \quad Nu_s = \frac{(x+b)q_w}{k(T_w-T_o)}$$

$$\tau_w = \left[ \left( \mu_{nf} + \frac{1}{\beta d} \right) \frac{\partial u}{\partial y} - \frac{1}{6\beta d^3} \left( \frac{\partial u}{\partial y} \right)^3 \right]_{y=a(x+b)\frac{1}{12}}$$

$$q_w = -k \left( \frac{\partial T}{\partial y} \right)_{y=a(x+b)\frac{1}{12}}$$

In dimensionless form we have[37,38]:

$$C_f \text{ Re}_s^{1/2} = \sqrt{2(n+1)} \left( 1 + N \right) f''(0) - \frac{(n+1) N \lambda}{2} \left( f''(0) \right)^3$$

$$N\mu_s \text{ Re}_s^{-1/2} = -\sqrt{\frac{n+1}{2}} \varphi'(0)$$

where $\text{Re}_s$ designates the local Reynolds number presented by $\frac{U_w(x+b)}{v}$.

3. SOLUTION OF THE PROBLEM:

The governing equations for the present problem are transformed into a set of coupled nonlinear differential equations by applying similarity transformation. The equations (16) - (18) together with the boundary conditions (19) – (20) are integrated numerically by using Runge-Kutta-Gill method along with the shooting technique. This method is concisely outlined as below:
The boundary conditions are transformed as follows:

\[ y_1(0) = \alpha \left( \frac{1-n}{1+n} \right), \quad y_2(0) = 1, \quad y_4(0) = 1, \quad y_6(0) = 1 \]

\[ y_2(\infty) = 0, \quad y_4(\infty) = 0, \quad y_6(\infty) = 0 \]  

In order to carry out the step by step integration for the equations (16) – (18), Gill’s procedures have been used (Ralston and Wilf [23]). To start the integration it is necessary to provide all the values of \( y_1, y_2, y_3, y_4, y_5, y_6 \) at \( \eta = 0 \) from which point, the forward integration has been carried out but from the boundary conditions it is seen that the values of \( y_3, y_5, y_7 \) are not known. So, we are to provide such values of \( y_3, y_5, y_7 \) along with the known values of the other function at \( \eta = 0 \) as would satisfy the boundary conditions as \( \eta \rightarrow \infty \) to a prescribed accuracy after step by step integrations are performed. Since the values of \( y_3, y_4, y_7 \) which are supplied are merely rough values, some corrections have to be made in these values in order that the boundary conditions to \( \eta \rightarrow \infty \) are satisfied. These corrections in the values of \( y_3, y_4, y_7 \) are taken care of by a self-iterative procedure which can for convenience be called corrective procedure.

4 RESULTS AND DISCUSSION:

In this section, we have presented the physical behavior of the velocity, temperature and concentration profiles for different physical parameters such as magnetic parameter \( M \), fluid parameters \( \lambda, N \), wall thickness parameter \( \alpha \), Prandtl number \( Pr \), heat source/sink parameter \( Q \), thermophoresis parameter \( Nt \), Brownian motion parameter \( Nb \) and thermal radiation parameter \( Nr \). we are solving the system of coupled nonlinear equations by using well known method Runge-Kutta-Gill method along with the shooting technique.
Fig. 2 portrays velocity field for varied values of magnetic parameter $M$, fluid parameters $\lambda$ and $N$. It is observed that velocity profiles reduce with an increase in magnetic parameter $M$, physically, presented results occurs in the conductivity fluid and create a resistive type force i.e. Lorentz force on the fluid in the boundary layer, which fall on the velocity of the fluid. In the presence of fluid parameter, it is noteworthy that the velocity profile depicts an increment with increasing $N$. Furthermore, the boundary layer is thicker for larger values of the fluid parameter $\lambda$. In real, larger values of $\lambda$ result in the reduction of fluid viscosity because of shear thinning property of the fluid, which enhance the molecular movement and results into increase of the velocity field. The behaviour of $M$, $N$ and $\lambda$ on the temperature and concentration is shown in figs. 3 and 4 respectively. Temperature and nano concentration profiles show increasing behaviour for higher values of $M$ and $\lambda$, whereas decreasing behaviour for $N$. An increment in $M$ produces higher Lorentz force (resistive force) which has the characteristic to convert some thermal energy into heat energy. Therefore the temperature and concentration profile increases. Furthermore, the opposite behaviour was observed for the effect of $N$. Physically, it justifies that higher value of $N$ produce a reduction in the fluid viscosity. Therefore, less heat is produced due to frictional force. Hence, the temperature and concentration distribution decreases.

Figs. 5, 6 & 7 displays that the wall thickness parameter $\alpha$ decreases velocity, temperature and nano concentration profile of the fluid. Physically, increasing the value of $\alpha$ decrease the flow velocity, because under the variable wall thickness, not all the pulling force of the stretching sheet can be transmitted to the fluid causing a decrease for both friction between the fluid layer and temperature and concentration distributions for the fluid. Furthermore, from the figure 6 and 7, it is observed that an increase in the Prandtl number results in decreasing the heat and mass transfer profiles. The reason is that increasing values of Prandtl number is equivalent to decreasing the thermal conductivities, and therefore heat is able to diffuse away from the heated sheet more rapidly. Hence, in the case of increasing Prandtl number the boundary layer is thinner and the heat transfer is reduced. Effects of the thermophoresis parameter $Nt$ and Brownian motion parameter $Nb$ on temperature and nano concentration distributions are shown in figures 8 and 9. It is comprehended that temperature and concentration fields are increasing functions of thermophoretic parameter. In fact, small particles are pulled towards cold surface from hot one. Eventually, temperature of the fluid increases which results in higher temperature and nano concentration profiles. From these figures, it also analyzed that temperature and concentration distributions show increasing and decreasing behaviour for higher values of Brownian motion parameter with upsurge in values of Brownian motion parameter an increase in fluid particles random motion is observed that eventually produce more heat. So, we observe increasing temperature field and decreasing
concentration distribution. The effects of radiation $Nr$ and heat source ($Q>0$) or sink ($Q<0$) on dimensionless temperature is exhibited in fig. 10. It is noteworthy here that $Nr = 0$ denotes no radiation and $Nr \neq 0$ show the presence of radiation. Clearly, dimensionless temperature is higher as $Nr$ increases. The reason behind this fact is that heat energy released to the fluid as $Nr$ increases and these results rise in temperature. It is also evident from this figure that thermal boundary layer thickness increases faster with increase in $Nr$. From this figure it is also noticed that temperature profiles increases with an increase in the heat source parameter and decreases for increasing strength of heat sink parameter. This is due to the fact that $(Q>0)$ generates the additional energy and this causes the increase in thickness of thermal boundary layers.

To verify the accuracy of the numerical results, we compared our results with those reported by Akbar et.al.[24] and Malik et.al.[25] (for regular fluids) as shown in table 1. The results are very good agreement, thus lending confidence to the accuracy of the present results. Table 2 depict the behavior of involved parameters $M, n, \lambda, \alpha$ and $N$ on skin friction coefficient. It is observed that skin friction coefficient increases for $M, n, \alpha$ and $N$ but decreases for $\lambda$. Thus higher values of $\lambda$ can be used for the reduction of the skin friction coefficient in different industrial processes in order to increase the efficiency of various machines. The effects of $Nt, Nb, Nr, Q, Pr$ and $Le$ (see table 3) is to generate more heat in the boundary layer region and hence to reduce the wall heat transfer rate but the influence of a Prandtl number is to enhance the wall heat transfer rate. Table 4 displays that the wall mass transfer rate increases with increase in the Brownian motion parameter, radiation parameter, heat source/sink parameter, Prandtl number and Lewis number.
Figure 3: Temperature profile for various values of $M$, $\lambda$ & $N$.

Figure 4: Concentration profiles for various values of $M$, $\lambda$ & $N$.

Figure 5: Velocity profile for various values of $\alpha$
Figure 6: Temperature profiles for various values of $\alpha$ & Pr.

Figure 7: Concentration profiles for various values of $\alpha$ & Pr.

Fig 8: Temperature profile for various values of $N_t$ & $Nb$
Figure 9: Concentration profile for various values of $Nt$ & $Nb$.

Figure 10: Temperature profiles for various values of $Nr$ and $Q$. 

$Nt = 0.1, 0.3, 0.5$

$n = 0.5$

$Pr = 2$

$Le = 2$

$N = 0.5$

$\lambda = 0.2$

$Nr = 0.5$

$\alpha = 0.5$

$Q = 0.2$
Table 1: Comparison of Skin-friction coefficient $C_f \text{Re}^{1/2}$ with the available results in literature for different values of $M$ when $n = \lambda = \alpha = 0$.

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Table 2: Numerical data of $-C_f \text{Re}^{1/2}$ for different parameters of involved parameters $M, n, \lambda, \alpha$ and $N$ when $Nt = Nb = 0.1, Nr = 0.5, Q = 0.2, Pr = Le = 2$.

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Table 3: Numerical values of $\frac{Nu_x}{Re}^{-1/2}$ for different parameters of involved parameters $Nt, Nb, Nr, Q, Pr$ and $Le$ when $M = n = \alpha = 0.5, \lambda = 0.2$. 

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Table 4: Numerical values of $\frac{Sh}{Re^{1/2}}$ for different parameters of involved parameters $Nt, N_b, N_r, Q, Pr$ and $Le$ when $M = n = \alpha = 0.5, \lambda = 0.2$.

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<th>$N_r$</th>
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5. CONCLUSIONS:

We inspected the feature of radiative Powell-Eyring nano fluid past a stretching sheet with variable thickness and heat source/sink. An increment in wall thickness parameter results in decrease of velocity, temperature and concentration profiles. Enhancement in the fluid temperature is observed for higher thermophoresis parameter. Temperature profile increases for increasing values of radiation parameter. Magnitude of both local Nusselt number and Sherwood numbers are decreasing functions of $Nr$ and increasing functions of $Pr$.

REFERENCES


