MIMO DC-DC Converter Fed Diode Clamped Multilevel Inverter: Design, Simulation and Analysis

C.Suganya[#], S.AugustiLindiya[#] and K.Vijayarekha[#]

Department of Electrical and Electronics Engineering, Sastra University

Thanjavur, Tamilnadu-613 401, India

suganyac4@gmail.com

Abstract

In this paper aMultiple Input Multiple Output(MIMO) topology capable of interfacing hybridized energy source with diode clamped multilevel inverter is designed, simulated and analyzed. The MIMO converter can accommodate multiple input sources and output load and has single inductor which is cost effective. By using single stage, two input two output DC-DC boost converter, regulated voltage in series is produced. Multiple output loads have different level of voltages, so voltage regulation across the output port is done using compensators. To design a controller for the converter system small signal modeling is done for each mode of operation and its performance is analyzed and verified using SISOTOOL(GUI). This series regulated output voltage is fed to diode clamped multilevel inverter to get a sinusoidal AC output voltage. Balancing of capacitor voltage and the use of multiple energy sources for Diode Clamped Multilevel Inverter (DCMI) is possible using MIMO DC-DC boost converter system.

Keywords:MIMO (Multi Input Multi Output) DC-DC boost converter, multilevel inverter, voltage regulation, small signal modeling, SISOTOOL.

Introduction

Use of renewable energy sources has been increasing day by day due to the limited supply of conventional energy sources. It also has numerous advantages such as sustainability, low environmental impacts and less maintenance. However, renewable energy sources have the problem of intermittent that is they are not available continuously eg. Solar and wind energy [1]. In order to overcome this problem different energy sources can be combined together through a multi input system such that the optimal utilization of each energy source can be made possible [2]-[4].

Multi input multi output DC-DC boost converter system is capable of combining multiple energy sources and provide multiple output voltages [5]. For an N number of output voltages the number of inductors required is also Nbut this type of converter system use only one inductor and a less number of switches are used [6]. Hence this leads to decrease in cost, size and switching loss. The most important application of this converter is that it can boost lower input voltages and regulate lower output voltages.

Inverters are needed to connect the converter system to the power grid. The main aim of industries is to have less production cost with high efficiency[7]-[9]. There are many types of inverter among them multilevel inverters are mostly required for industries because of its medium and high power operation with reduced harmonic distortion [10]. As the number of levels increases, the output waveform produced will have more steps so that a fine staircase waveform closer to sine waveform is obtained. Among the various multilevel inverter types, diode clamped multilevel inverter is the most widely used multilevel inverters since it has high efficiency for the fundamental switching frequency [11]. It also has lower number of capacitors which leads to low cost, weight and volume. Use of diode clamped multilevel inverter has the following [12] disadvantages,

- 1. Balancing of capacitor voltage.
- 2. Use of multiple energy sources.

MIMO DC-DC boost converter can solve this problem and simplify the control strategy [14],[15]. The overall block diagram for diode clamped multilevel inverter fed from MIMO DC-DC boost converter is shown in Figure 1. MIMO converter accepts multiple energy sources simultaneously and gives multiple outputs. This paper presents a dual input dual output converter system. In order to maintain a constant output voltage a controller is used. This series regulated voltage obtained across the capacitor is fed to diode clamped multilevel inverter to get a sinusoidal AC output voltage and then can be connected to the load.

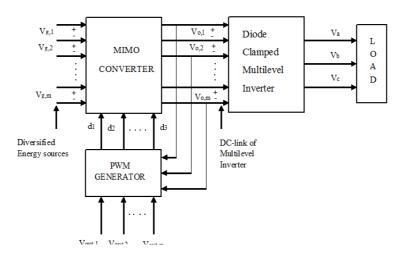


Figure 1:Block diagram for the proposed system

Converter Configuration

Circuit diagram for two input two output DC-DC boost converter is shown in Figure 2. It consist of two input sources V_{in1} and V_{in2} with the condition $V_{in1} < V_{in2}$ such that the operation can be simplified. It has three switches $(S_1, S_2 \text{ and } S_3)$, three diodes $(D_0, D_1 \text{ and } D_2)$ and two capacitors $(C_1 \text{ and } C_2)$.

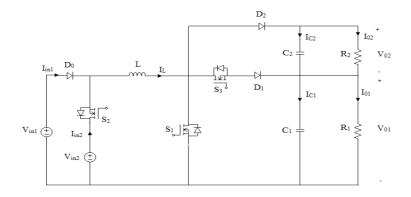


Figure 2:Twoinput two output DC-DC boost converter

Pulses for the switches and voltage and current waveforms across the inductor is shown in Figure 3. According to the switching pattern there are four different modes of operation which are explained in Table 1.

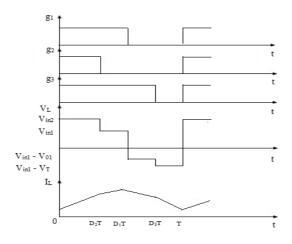


Figure 3: Steady state waveforms of the proposed converter

Switching state	Interval	S_1	S_2	S_3	C ₁	C ₂	$I_{ m L}$
1	$0 < t < D_2T$	ON	ON	OFF	Discharges	Discharges	Increases
2	$D_2T < t < D_1T$	ON	OFF	OFF	Discharges	Discharges	Increases
3	$D_1T < t < D_3T$	OFF	OFF	ON	Charges	Discharges	Decreases
4	$D_2T < t < T$	OFF	OFF	OFF	Charges	Discharges	Decreases

Table 1: Switching states of dual input dual output DC-DC boost converter

Use of control technique for the proposed converter is to produce regulated voltage across the DC link capacitor which automatically avoids the capacitor voltage unbalancing of diode clamped multilevel inverter. Therefore, by using two input two output converter system the control strategy for diode clamped multilevel inverter is simplified and use of multiple energy sources is possible. Figure 4 shows the circuit diagram for DCMI.

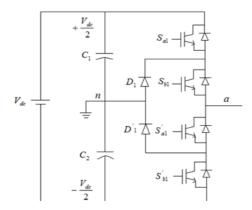


Figure 4: Three level diode clamped multilevel inverter

Dynamic Modeling of The Converter

According to the small signal modeling method the input voltages, duty ratios and the state variableshave its DC values and perturbations. Thus, based on state space averaging method applied to the equations obtained from four different modes of operation, equation (1) is obtained.

$$L\frac{d\hat{i}_{L}}{dt} = (V_{in2} - V_{in1}) \hat{d}_{2}(t) + D_{2}\hat{v}_{in2}(t) + (1 - D_{2}) \hat{v}_{in1}(t) - (1 - D_{1}) \hat{v}_{01}(t) + (D_{3} - 1)$$

$$\hat{v}_{02}(t) + V_{01}\hat{d}_{1}(t) + V_{02}\hat{d}_{3}(t)$$

$$C1\frac{d\hat{v}_{01}(t)}{dt} = -I_{L}\hat{d}_{1}(t) + (1 - D_{1}) \hat{i}_{L}(t) - \frac{\hat{v}_{01}(t)}{R_{1}}$$

$$(1)$$

$$C_2 \frac{d\hat{v}_{02}(t)}{dt} = -I_L \hat{d}_3(t) + (1 - D_3)\hat{i}_L(t) - \frac{\hat{v}_{02}(t)}{R_2}$$

Switching period for S_1 , S_2 and S_3 are found from equation (3) which is the steady state equation.

$$\begin{bmatrix} V_{01} & V_{in2} - V_{in1} & V_{02} \\ R_{1}I_{b} & V_{01} & 0 \\ 0 & V_{02} & R_{2}I_{b} \end{bmatrix} \begin{bmatrix} D_{1} \\ D_{2} \\ D_{3} \end{bmatrix} = \begin{bmatrix} V_{02} + V_{01} - V_{in1} \\ R_{1}I_{b} \\ R_{2}I_{b} \end{bmatrix}$$
(2)

The state space model of the proposed converter is given in the equation (3) and (4).

$$\begin{bmatrix} \hat{\mathbf{i}}_{L} \\ \hat{\mathbf{v}}_{01} \\ \hat{\mathbf{v}}_{02} \end{bmatrix} = \begin{bmatrix} 0 & \frac{(\mathbf{D}_{1} - \mathbf{l})}{L} & \frac{(\mathbf{D}_{3} - \mathbf{l})}{L} \\ \frac{(\mathbf{l} - \mathbf{D}_{I})}{C_{1}} & \frac{-1}{R_{1}C_{1}} & 0 \\ \frac{(\mathbf{l} - \mathbf{D}_{3})}{C_{2}} & 0 & \frac{-1}{R_{2}C_{2}} \end{bmatrix} \begin{bmatrix} \hat{\mathbf{i}}_{L} \\ \hat{\mathbf{v}}_{01} \\ \hat{\mathbf{v}}_{02} \end{bmatrix} + \begin{bmatrix} \frac{\mathbf{V}_{02}}{L} & \frac{\mathbf{V}_{01}}{L} & \frac{(\mathbf{V}_{in2} - \mathbf{V}_{in1})}{L} \\ 0 & \frac{-\mathbf{I}_{L}}{C_{1}} & 0 \\ \frac{-\mathbf{I}_{L}}{C_{2}} & 0 & 0 \end{bmatrix} \begin{bmatrix} \hat{\mathbf{d}}_{3} \\ \hat{\mathbf{d}}_{1} \\ \hat{\mathbf{d}}_{2} \end{bmatrix}$$
(3)

$$\begin{bmatrix} \hat{\mathbf{v}}_{01} \\ \hat{\mathbf{v}}_{T} \\ \hat{\mathbf{I}}_{in2} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 1 & 1 \\ D_{3} & 0 & 0 \end{bmatrix} \begin{bmatrix} \hat{\mathbf{i}}_{L} \\ \hat{\mathbf{v}}_{01} \\ \hat{\mathbf{v}}_{02} \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & \mathbf{I}_{L} & 0 \end{bmatrix} \begin{bmatrix} \hat{\mathbf{d}}_{3} \\ \hat{\mathbf{d}}_{1} \\ \hat{\mathbf{d}}_{2} \end{bmatrix}$$

$$(4)$$

The transfer functions are obtained as,

$$g_{11} = \frac{\hat{v}_{01}(s)}{d_3(s)}$$

$$= \frac{\left(\frac{V_{02}(1-D_{l})}{LC_{l}}\right)S + \left(\frac{(1-D_{l})V_{02}}{LR_{2}C_{1}C_{2}} - \frac{(1-D_{l})(D_{3}-l)I_{L}}{LC_{1}C_{2}}\right)}{S^{3} + \left(\frac{R_{1}C_{1} + R_{2}C_{2}}{R_{1}R_{2}C_{1}C_{2}}\right)S^{2} + \left(\frac{L + (1-D_{l})^{2}R_{1}R_{2}C_{2} + (D_{3}-l)^{2}R_{1}R_{2}C_{1}}{LR_{1}R_{2}C_{1}C_{2}}\right)S + \left(\frac{R_{1}(1-D_{l})^{2} + (D_{3}-l)^{2}R_{2}}{LR_{1}R_{2}C_{1}C_{2}}\right)}$$
(5)

$$g_{22} = \frac{\hat{v}_{T}(s)}{d_{2}(s)}$$

$$= \frac{\left(\frac{V_{in2} - V_{in1}}{L}\right) \left(\frac{\left(1 - D_{l}\right)}{C_{l}} - \frac{D_{3} - 1}{C_{2}}\right) S + \left(\frac{\left(1 - D_{l}\right)}{R_{2}C_{l}C_{2}} - \frac{\left(D_{3} - 1\right)}{R_{l}C_{l}C_{2}}\right) \left(\frac{V_{in2} - V_{in1}}{L}\right)}{S^{3} + \left(\frac{R_{l}C_{1} + R_{2}C_{2}}{R_{l}R_{2}C_{1}C_{2}}\right) S^{2} + \left(\frac{L + \left(1 - D_{l}\right)^{2}R_{l}R_{2}C_{2} + \left(D_{3} - 1\right)^{2}R_{l}R_{2}C_{l}}{LR_{l}R_{2}C_{1}C_{2}}\right) S + \left(\frac{R_{l}(1 - D_{l})^{2} + \left(D_{3} - 1\right)^{2}R_{2}}{LR_{l}R_{2}C_{1}C_{2}}\right)$$
(6)

$$g_{33} = \frac{I_{in2}(s)}{d_1(s)}$$

$$=\frac{\left(\frac{V_{01}D_{2}}{L}\right)S^{2} + \left(\frac{D_{2}V_{01}}{L}\left(\frac{1}{R_{1}C_{1}} + \frac{1}{R_{2}C_{2}}\right) + \frac{I_{L}(1-D_{1})D_{2}}{LC_{1}}\right)S + \left(\frac{D_{2}V_{01}}{LR_{1}R_{2}C_{1}C_{2}} + \frac{I_{L}(1-D_{1})D_{2}}{LR_{2}C_{1}C_{2}}\right)}{S^{3} + \left(\frac{R_{1}C_{1} + R_{2}C_{2}}{R_{1}R_{2}C_{1}C_{2}}\right)S^{2} + \left(\frac{L + (1-D_{1})^{2}R_{1}R_{2}C_{2} + (D_{3}-1)^{2}R_{1}R_{2}C_{1}}{LR_{1}R_{2}C_{1}C_{2}}\right)S + \left(\frac{R_{1}(1-D_{1})^{2} + (D_{3}-1)^{2}R_{2}}{LR_{1}R_{2}C_{1}C_{2}}\right)}$$

$$(7)$$

Thus from the transfer functions (5), (6) and (7)it is obviously seen that the output voltages V₀₁ and V_T are controlled by controlling the duty cycles d₃ and d₂ respectively. The specifications which are designed and used in the model are given in Table 2.

Parameters	Values		
Input voltage 1 (V _{in1})	24V		
Input voltage 2 (V _{in2})	36V		
Inductor (L)	28mH		
Capacitor (C ₁ and C ₂)	1000μF and 2200μF		
Resistor (R ₁ and R ₂)	35Ω and 35Ω		
Switching Frequency (f _{sw})	10kHZ		
Output Voltage (V ₀₁)	80V		
Output Voltage (V ₀₂)	40V		

Table 2: Specifications of two input two output DC-DC boost converter

The values specified in Table 2 are substituted in the transfer functions g_{11}, g_{22} and is obtained as,

$$g_{11} = \frac{\hat{\mathbf{v}}_{01}(\mathbf{s})}{\mathbf{d}_{3}(\mathbf{s})} = \frac{396428.57S + 10262059.37}{S^{3} + 41.558S^{2} + 3950.60S + 52179.96}$$
(8)

$$g_{11} = \frac{\hat{\mathbf{v}}_{01}(s)}{\mathbf{d}_{3}(s)} = \frac{396428.57S + 10262059.37}{S^{3} + 41.558S^{2} + 3950.60S + 52179.96}$$

$$g_{22} = \frac{\hat{\mathbf{v}}_{T}(s)}{\mathbf{d}_{2}(s)} = \frac{157791.68S + 2504636.54}{S^{3} + 41.558S^{2} + 3950.60S + 52179.96}$$
(9)

Control Strategy

The need for control system design of MIMO DC-DC boost converter system is to maintain the constant output voltage. Compensators are one of the best controllers. Using compensators stability of the system can be increased and the steady state error can be eliminated. Lead, Lag, Lead/Lag are the types of compensators. These are designed in the form of transfer functions using SISO tool in MATLAB Simulink. Using the transfer functions g_{11} and g_{22} obtained from small signal modeling method, for switches S_2 and S_3 compensators can be designed. Bode plot obtained before applying compensator for g_{11} is shown in Figure 5a. The phase margin of the system obtained is low so to increase the phase margin a lead compensator is designed using frequency response and is given in equation (10).

$$G_{11}(s) = 1000 \frac{(S+1)}{(S+21200)}$$
 (10)

Bode plot obtained after applying compensator for g_{11} is shown in Figure 5b. Thus the phase margin of the system and system stability is improved.

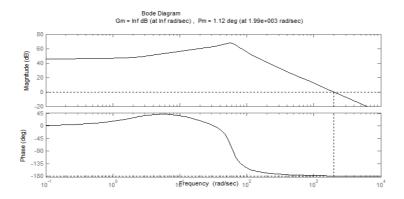


Figure5a: Bode plot of g₁₁ obtained before applying compensator

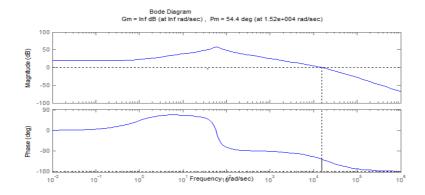


Figure5b: Bode plot of g_{11} obtained after applying compensator

Bode plot obtained for g_{22} before applying compensator is shown in Figure 6a. This figure shows that the phase margin of the system obtained is low so to increase the phase margin a lead compensator is designed using frequency response and is given in equation (11).

$$G_{22}(s) = 9 \frac{(S+15)}{(S+1000)}$$
 (11)

Bode plot obtained after applying compensator for g_{22} is shown in Figure 6b. Thus the phase margin of the system and system stability is improved.

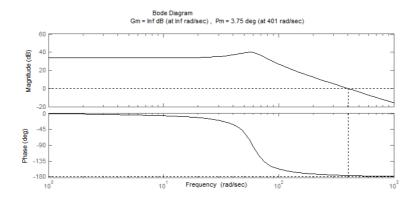


Figure6a: Bode plot of g₂₂ obtained before applying compensator

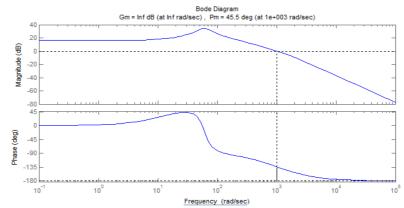


Figure6b: Bode plot of g₂₂obtained after applying compensator

Simulation Results

The performance of the proposed converter has been verified using MATLAB Simulink software. The converter system has two input voltage sources $V_{\rm in1}$ and $V_{\rm in2}$ of 24V and 36V respectively connected through various switches and an inductor. The converter system produces regulated output voltages in series andis fed to the inverter. Simulation results across the inductor of the converter is measured and obtained as shown in Figure 7.

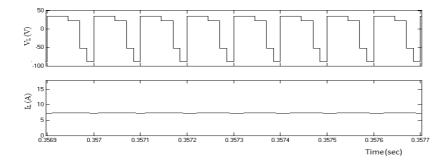


Figure 7: Simulation results across the inductor of the converter

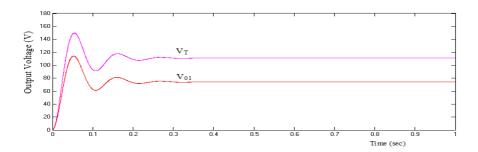


Figure8:Output voltage waveform of the converter under open loop condition

The output voltages measured across the converter is shown in Figure 8. Since it is boost converter the total output voltage required to obtain is 120V that is 80V and 40V across the loads R_1 and R_2 respectively but only 76V and 34V is obtained. So to produce a series regulated output voltage controllers are used. The simulation results of closed loop control fortwo input two output DC-DC boost converter is shown in Figure 9.

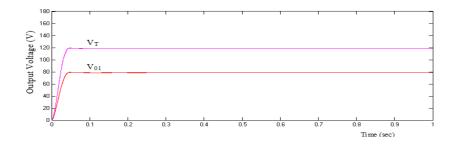


Figure9:Output voltage waveforms of the converter under closed loop condition

In order to verify the performance of controller disturbances are given to load current. Figure 10 shows that under closed loop condition even though disturbances are given the output voltage is maintained constant, but it takes 0.1 Sec to settle.

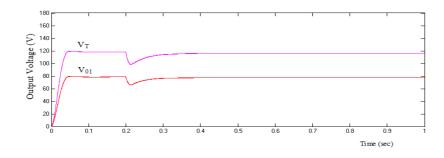


Figure 10: Output voltage waveforms of the converter under disturbances

Three phase three level multilevel inverters is designed to interface with MIMO DC-DC boost converter. Simulation results forthephaseand line voltageof diode clamped multilevel inverter fed from two input two output DC-DC boost converter is shown in Figure 11 and Figure 12respectively.

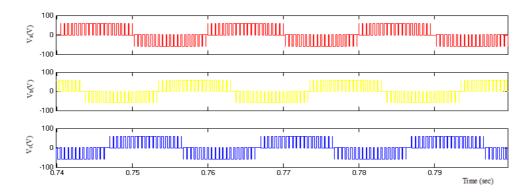


Figure 11: Phase voltage of diode clamped multilevel inverter fed from two input two output DC-DC boost converter

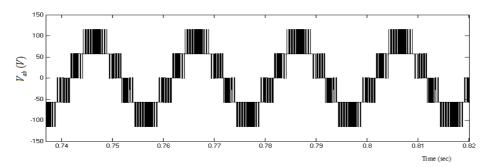


Figure 12:Line voltage (V_{ab}) of diode clamped multilevel inverter fed from two input two output DC-DC boost converter

Conclusion

This paper proposes a diode clamped multilevel inverter fed from MIMO DC-DC boost converter. Using two input two output DC-DC boost converter two different energy sources have been combined by which two different output voltages are produced. Its different modes of operation, steady state and dynamic characteristics has been studied. Controllers for the converter system using small signal modeling is designed and closed loop operation for MIMO converter has been performed. This MIMO converter is fed to diode clamped multilevel inverter with a DC link capacitor as an intermediate. Thus multiple energy sources are fed to diode clamped multilevel inverter and its capacitor voltage imbalance is reduced.

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