Experimental investigation of Surface roughness of cylinder liner for HT 100 material using RSM Technique

Mr. B.N. Tripathi

Research Scholar Deptt. of Mech. Engg. ISM Dhanbad India

Dr. N.K. Singh

Associate Professor (Workshop) Deptt. of Mech. Engg ISM Dhanbad India

Abstract

Surface roughness of any manufactured components is an important and valuable performance measured, as for as theoretical and practical applications are concern. It is widely used as an index of product quality and is in most cases a technical requirement for mechanical products. Surface roughness is an important design consideration as it impacts many part characteristics such as fatigue strength, assembly tolerances, coefficient of friction, wear rate, corrosion resistance and aesthetics. In the present study honing process is done on the HT 100 and the response surface methodology is used to validate the results.

Keywords: Honing Process, Surface roughness, RSM technique.

Introduction Surface Roughness

The concept of surface texture has previously varied according to whether a scientist, technologist, or engineer has inspected a surface. Surface technology encompasses a wide range of disciplines that include: metrology, metallurgy, material science, physics, chemistry and mechanical design (Staut, 1984). Surface roughness affects mechanical and even electrical properties of a given component such as electrical capacity, electronic conductivity, surface energy, critical areas, peak electrical field, surface tension, and sheet resistance. Surface finish in fact determines the performance and reliability of many products (Kardar, 2000). The surface is the final link from the original design concept through its manufacture, with the industrial engineer being the last person to add value to the product prior to shipment (PDI Webmaster, 2004). Surface roughness is a quantitative measure of the marks produced by the process of creation of the surface. Other factors such as the structure of the material also influence roughness of the surface. Waviness or lay has longer wavelength and is related to the vibration of the finishing machine. Industry is continually trying to improve component power-to-weight ratios, drive down manufacturing costs and find efficient ways of either producing or improving surfaces. This has become an established goal of world-class competing companies. Regardless of the method of manufacture, an engineering surface must have some form of texture associated with it, this being a combination of several interrelated factors, such as microstructure of the material of component, the surface generation method, cutting action of the tool, tool geometry, cutting speed, feed rate, and application of cutting fluid, instability during the manufacturing process, and residual stress produced by stress patterns often causing deformations in the component (Mantle and Aspinwall, 2001).

Honing Process

Honing is a fine finishing abrasive machining process with a multi-edge cutting tool of bonded grains under constant surface contact between tool and pre-machined components, which offers good geometrical tolerances (Kalpakijan and Schmid, 2003). It is a controlled, low speed sizing and surface finishing process in which stock is removed by the shearing and plugging action. Selection of honing stone and grit size depends mainly on the desired rate of metal removal and the required finish. Abrasive material of the hone is chosen on the basis of the composition and hardness of the metal being honed and the finish required. The selection of a particular honing machine depends on the size and shape of the work piece, number of pieces to be honed, tolerance requirement, availability of equipment, and availability of skilled workers. Honing provides a cost effective alternative to other finishing processes like grinding, lapping and super finishing (Leon, 2002).

Response Surface Methodology

Response Surface Methodology (RSM) is a collection of statistical and mathematical techniques useful for developing, improving, and optimizing processes.

The most extensive applications of RSM are in the particular situations where several input variables potentially influence some performance measure or quality characteristic of the process. Thus performance measure or quality characteristic is called the response. The input variables are sometimes called independent variables, and they are subject to the control of the scientist or engineer. The field of response surface methodology consists of the experimental strategy for exploring the space of the process or independent variables, empirical statistical modelling to develop an appropriate approximating relationship between the yield and the process variables, and optimization methods for finding the values of the process variables that produce desirable values of the response. In this report we will concentrate on the second strategy: statistical modelling to develop an appropriate approximating model between the response y and independent variables $\xi_1, \xi_2, ..., \xi_K$.

$$y = f(\xi_1, \xi_2,...,\xi_K) + \epsilon;$$
 (1)

where the form of the true response function f is unknown and perhaps very complicated, and ε is a term that represents other sources of variability not accounted for in f. Usually ε includes effects such as measurement error on the response, background noise, the effect of other variables, and so on. Usually ε is treated as a statistical error, often assuming it to have a normal distribution with mean zero and variance (σ^2). The true response function f is unknown, we must approximate it. In fact, successful use of RSM is critically dependent upon the experimenter's ability to develop a suitable approximation forf. usually, a low-order polynomial in some relatively small region of the independent variable space is appropriate. In many cases, either a first-order or a second order model is used. The first-order model is likely to be appropriate when the experimenter is interested in approximating the true response surface over a relatively small region of the independent variable space in a location where there is little curvature in f. This is the first-order model with interaction. Adding the interaction term introduces curvature into the response function.

Often the curvature in the true response surface is strong enough that the first-order model (even with the interaction term included) is inadequate. A second-order model will likely be required in these situations. For the case of two variables, the second-order model is give as-

$$\eta = \beta o + \beta_1 x_1 + \beta_2 x_2 + \beta_1 x_1^2 + \beta_2 x_2^2 + \beta_1 x_1 x_2;$$
(2)

This model would likely be useful as an approximation to the true response surface in a relatively small region. The second-order model is widely used in response surface methodology for several reasons:

- 1. The second-order model is very flexible. It can take on a wide variety of functional forms, so it will often work well as an approximation to the true response surface.
- 2. It is easy to estimate the parameters (the β 's) in the second-order model. The method of least squares can be used for this purpose.
- 3. There is considerable practical experience indicating that second-order models work well in solving real response surface problems.

Sequential Nature of Response Surface Methodology

Most applications of RSM are sequential in nature.

Phase 0: At first some ideas are generated concerning which factors or variables are likely to be important in response surface study. It is usually called a screening experiment. The objective of factor screening is to reduce the list of candidate variables to a relatively few so that subsequent experiments will be more efficient and require fewer runs or tests. The purpose of this phase is the identification of the important independent variables.

Phase 1: The experimenter's objective is to determine if the current settings of the independent variables result in a value of the response that is near the optimum. If the current settings or levels of the independent variables are not consistent with optimum performance, then the experimenter must determine a set of adjustments to the process variables that will move the process toward the optimum. This phase of RSM makes

considerable use of the first-order model and an optimization technique called the method of steepest ascent (descent).

Phase 2: Phase 2 begins when the process is near the optimum. At this point the experimenter usually wants a model that will accurately approximate the true response function within a relatively small region around the optimum. Because the true response surface usually exhibits curvature near the optimum, a second-order model (or perhaps some higher-order polynomial) should be used. Once an appropriate approximating model has been obtained, this model may be analyzed to determine the optimum conditions for the process. This sequential experimental process is usually performed within some region of the independent variable space called the operability region or experimentation region or region of interest.

RSM as an Automated Tool for Modelling & Validation

Modern computational large scale social networks simulation systems are becoming heavily used due to their efficiency and flexibility in modelling and simulation of complex social networks. Since these models are increasing in complexity and size they require more significant time and efforts for their validation, optimization, improvement and understanding of their behaviour. One example of such multi-agent socialnetwork model named Bio War is presented spatial city-scale multi-agent social-network model capable of simulating the effects of biological weapon attacks against the background of naturally-occurring diseases on demographically realistic population. Response Surface Methodology (RSM) might be extremely useful as an automated tool that can be used to calibrate such multi-agent models as Bio War, and facilitate validation and understanding, thereby increasing model fidelity and reliability and giving the user some feedback for analysis and insight.

Every simulation model has its own specific that should be taken into consideration when we try to specify independent and dependent variables. For example, within ORA the RSM tool can use one group of measures like a person's height, age, weight as independent variables and another like the amount of money earned as the dependent variable. We can also consider some of DNA measures like Resource Congruence or Task Exclusivity as independent variables while some other DNA measure like Network Closeness Centralization can serve as dependent variable. If the RSM is operating on the node level measures then independent variables can be any node level measure. There is a particular interest also in consideration of some means or standard deviations of the graph level measures as dependent or independent variables. The RSM is also useful for searching the input combination

The RSM is also useful for searching the input combination that maximizes the output of areal system or its simulation such as Bio War or ORA. When validating or optimizing a stochastic simulation model, one tries to estimate the model parameters that optimize specific stochastic output of the simulation model. A simulation framework is especially intended for simulation models where the calculation of the corresponding stochastic objective function is very expensive or time-consuming. RSM is frequently used for the optimization of stochastic simulation models. This methodology is based on approximation of the stochastic

objective function by a low order polynomial on a small sub region of the domain. The coefficients of the polynomial are estimated by ordinary least squares method applied to a number of observations of the stochastic objective function. To this end, the objective function is evaluated in an arrangement of points referred to as an experimental design. Based on the fitted polynomial, the local best point is derived, which is used as a current estimator of the optimum and as a centre point of a new region of experimentation, where again the stochastic objective function is approximated by a low order polynomial. In non-automated optimization, RSM is an interactive process in which the user gradually gains understanding of the nature of the stochastic objective function. In an automated RSM algorithm, however, human intervention during the optimization process is excluded. A good automated RSM algorithm should therefore include some degree of self-correction mechanisms factors as noise factors. RSM assumes that these noise factors are uncontrollable in the field, but can be controlled during process development for purposes of a designed experiment Considerable attention has been focused on the methodology advocated by Taguchi, and a number of flaws in his approach have been discovered.

Experimental setup:

Honing is an abrasive machining process that produces a precision surface on a metal work piece by scrubbing an abrasive stone against it along a controlled path. Honing is primarily used to improve the geometric form of a surface, but may also improve the surface texture. The honing process is used to obtain precise dimensions and surfaces in cylindrical shapes with a wide range of diameters. This applies to parts such as Hydraulic Cylinders, Pistons, Bearing Bores, Pin Holes and to some external cylindrical surfaces. The honing process offers advantages of low capital equipment cost, high metal removal rates, and extreme accuracy of 0.001mm (0.00004") in a wide variety of materials. Honing machines are available in a wide range of sizes and designs, in both horizontal and vertical types. They may be equipped with either manual stroking or power stroking mechanisms. Size and shape of the work piece are usually the major factors that determine whether manual or power stroking is more appropriate. Other relevant factors are the quantity of similar pieces to be honed, tolerance requirements, availability of skilled operators, and specific plant policies. Most bores honed by manual stroking are 25 mm in diameter or less, although bores up to about 127 mm in diameter have been successfully finished. The bore diameter of the cylinder liner chosen for the present study 47 mm. Power stroking with automatic control is used in preference for large quantities when tolerances are extremely close and size and shape of the work piece permit it. One advantage of manual stroking is that work pieces need not be held in a fixture, which reduces tooling investment and permits immediate changeover from one job to another. Automatic honing operation is the best technique than manual, who can instantly gage the part, close tolerances can be obtained. Techniques used to obtain the required accuracy required include end for end reversal of the work piece and change of stroke length.

In automatic power stroking, the machine rotates the tool at a preset speed as control parameters feed in to the control units. Because the axis of the honing tool is horizontal, stroking is also horizontal. These machines may be equipped with devices for controlled feed out of the honing stones. The manufacturing plant, where experiments for the present study were conducted, utilized a vertical type power stroking honing machine for finishing the liner bore. The experiments were run on a CNC operated honing machine, model HONSD,SL NO-210, (F:08:0023:02) having the facilities to hold the work piece within the place provided by the help of fixture, sketched shown in Fig. 1. Technical specifications of the above honing machine are given in the Table 1. The above machine rotated the honing tool at a pre-established speed while the work piece had lateral movement. It was stroked back and forth over the tool. The machine was equipped with devices for controlled feed out of the honing stones.

The operator loads the job on the hone tool and presses the pedal. The honing tool starts rotating and operator reciprocates the job manually. This manual cycle is continued till the time set for honing is over. Different types and grits of stones are used depending upon the material removal and surface finish requirement.

TABLE 1: Technical specifications of HONS 210

MODEL	HONSD,SL NO-210, (F:08:0023:02)			
Honing Operation	Power Stroking			
Capacity: Diameter	13-85 mm			
Capacity: Length	250 mm			
Spindle speed	250-1660 rpm			
Reciprocation speed	Automatic, CNC controlled			
Spindle drive motor	1.5HP. 1660 rpm			





 $Fig.\ 1: Honing\ Head\ with\ Tooling\ (Honda\ Ltd.\ Gurgaon)$

The operating cycle is repeated from part to part. The expanding mechanism of the honing tool is set for size on the first part and, except for a slight advance of the stone to compensate for wear; additional parts require no resetting of controls. Honing stones are also known as honing sticks. Honing stones used in the present study had grits of aluminums oxide bonded together with vitrified clay,

resinous, cork, carbon, or metal. The abrasive particles, or grits, which provide the cutting action, are able to withstand the pressure required for removing the excess metal from the bore. The bond is strong enough to hold the grit, but not too hard to excessively retard cutting action. The hardness and type of bond are indicated by code letters in the identification of the stone. The porosity of the honing stone, which facilitates chip clearance and minimizes heat generation, is controlled during molding.

Selection of abrasive for the stones depends mainly on the composition and hardness of the metal being honed, the finish required and the cost. Aluminum oxide and silicon carbide stones are comparable in initial cost. However, one may be more economical than the other because of increased service life. Aluminum oxide abrasive has been selected for honing the work piece materials HT 100 used for the chosen part. The range of the grits used for the experiments lies between 400-1000.

Experimental Procedure:

- 1. Mandrel, adaptor and stone are assembled and mounted in the chuck of the machine.
- Machine is switched on and speed control is set to the required value.
- 3. Stone feed is set at the chosen value.
- 4. Honing stone is fully retracted by rotating feed wheel anti-clockwise.
- 5. Honing fluid flow is adjusted and environmental temperature maintained as per requirement using Air-conditioning plant.
- 6. Cylinder liner is placed on the mandrel. Feed is adjusted until the clock shows a reading as per the desired value.
- 7. Stone feed is wound by the amount needed to produce size, i.e. equal to the honing allowance.
- 8. Start the spindle rotating and power stroking up to the time set for honing.
- 9. Remove the work piece after honing for the given time, at rated speed.
- 10. Repeat the process for another set for readings by changing the parameters as per the design of experiments.

Experimental Observations

Factors and levels of experiment for modeling

Five levels of each parameter (including positive and negative value of alpha) were taken for the model construction. Three (03) different set of experiments (readings) were conducted on the same level. Three different set of experiments were conducted on each material cylinder liner as per the DOE, which able to capture non-linear effects using Design Expert 8. The values of factor levels in different sets of experiments are listed in Table 2 through 4

TABLE 2: HT 100-Factors and levels for 1st set of readings

Size			·		1			I _	_
(µm) Temp. (°C) (RPM) (Deg.) (Bar) (Sec.)	SL	Grit	Environ			Fluid	Honing 	_	Power
1 43 40 600 60 9 60 325 1.8 2 68 10 600 20 4 60 456 3.6 3 68 10 600 20 9 30 529 3.7 5 68 10 600 60 4 30 276 1.5 5 68 10 600 20 4 30 276 1.5 6 43 10 600 20 4 30 303 2.2 8 56 25 900 40 6.5 45 388 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 60 9 60 502 3.8 12 <							(nm)	(KW)	
2 68 10 600 20 4 60 456 3.6 3 68 10 600 20 9 30 529 3.7 4 43 10 1200 60 4 30 276 1.5 5 68 10 600 60 4 30 433 2.9 6 43 10 600 20 4 30 303 2.2 8 56 25 900 40 6.5 45 388 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 60 9 30 422 3.3 13 68 10 1200 60 9 60 506 2.2 16	_	** *	• • •	•		•		225	4.0
3 68 10 600 20 9 30 529 3.7 4 43 10 1200 60 4 30 276 1.5 5 68 10 600 60 4 30 433 2.9 6 43 10 600 20 4 30 436 1.7 7 43 40 1200 20 4 30 303 2.2 8 56 25 900 40 6.5 45 388 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.3 13 68 10 1200 20 9 60 522 3.8 13 48 10 1200 20 9 60 526 2.2 16	_					_			
4 43 10 1200 60 4 30 276 1.5 5 68 10 600 60 4 30 433 2.9 6 43 10 600 20 4 30 436 1.7 7 43 40 1200 20 4 30 303 2.2 9 56 25 900 40 6.5 45 388 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 20 4 30 452 3 14 68 10 1200 60 9 60 502 2.8 15 43 40 1200 20 9 60 202 2.2 16	_								
5 68 10 600 60 4 30 433 2.9 6 43 10 600 20 4 30 446 1.7 7 43 40 1200 20 4 30 303 2.2 8 56 25 900 40 6.5 45 388 3.1 10 56 25 900 40 6.5 45 370 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 60 9 30 422 3.3 13 68 10 1200 20 9 60 5026 2.2 16 8 40 1200 20 9 60 296 2.2 16	_					_			
6 43 10 600 20 4 30 446 1.7 7 43 40 1200 20 4 30 303 2.2 8 56 25 900 40 6.5 45 388 3.1 9 56 25 900 40 6.5 45 381 3 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 20 4 30 452 3 13 68 10 1200 60 9 30 422 3.3 14 68 10 1200 20 9 60 526 4.3 15 43 40 1200 60 9 60 526 4.3 16	_								
7 43 40 1200 20 4 30 303 2.2 8 56 25 900 40 6.5 45 388 3.1 9 56 25 900 40 6.5 45 370 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 20 4 30 452 3 13 68 10 1200 60 9 30 422 3.3 14 68 10 1200 20 9 60 502 3.8 15 43 40 1200 60 9 60 202 2.2 16 68 40 1200 60 9 60 310 2.6 19	_								
8 56 25 900 40 6.5 45 388 3.1 9 56 25 900 40 6.5 45 370 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 20 4 30 452 3.3 14 68 10 1200 20 9 60 502 3.8 15 43 40 1200 20 9 60 296 2.2 16 68 40 1200 60 9 60 526 4.3 17 68 40 1200 60 9 60 526 4.3 18 43 10 1200 60 9 60 310 2.6 20 <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	_								
9 56 25 900 40 6.5 45 370 3.1 10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 20 4 30 452 3 13 68 10 1200 20 9 60 502 3.8 14 68 10 1200 20 9 60 502 3.8 15 43 40 1200 20 9 60 526 2.2 16 68 40 600 20 4 30 363 3.3 17 68 40 1200 60 9 60 310 2.6 19 68 10 1200 60 9 60 310 2.8 20									
10 56 25 900 40 6.5 45 381 3 11 68 40 600 60 4 60 519 3.9 12 68 10 1200 20 4 30 452 3 13 68 10 1200 60 9 30 422 3.3 14 68 10 1200 20 9 60 506 286 22 16 68 40 1200 20 9 60 296 22 16 88 40 1200 60 9 60 526 4.3 18 43 10 1200 60 9 60 310 2.6 19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 368 2.9	_								
11 68 40 600 60 4 60 519 3.9 12 68 10 1200 20 4 30 452 3 13 68 10 1200 20 9 60 502 3.8 14 68 10 1200 20 9 60 502 3.8 15 43 40 1200 20 9 60 502 2.2 16 68 40 600 20 4 30 363 3.3 17 68 40 1200 60 9 60 526 4.3 18 43 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 1200 20 9 30 553 3.5 24 <td>9</td> <td></td> <td>25</td> <td>900</td> <td>40</td> <td>6.5</td> <td>45</td> <td>370</td> <td>3.1</td>	9		25	900	40	6.5	45	370	3.1
12 68 10 1200 20 4 30 452 3 13 68 10 1200 60 9 30 422 3.3 14 68 10 1200 20 9 60 502 3.8 15 43 40 1200 20 9 60 296 2.2 16 68 40 600 20 4 30 363 3.3 17 68 40 1200 60 9 60 310 2.6 19 68 10 1200 60 9 60 310 2.6 19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 368 2.9 21 68 40 1200 20 9 30 553 3.5 25 <td>10</td> <td>56</td> <td>25</td> <td>900</td> <td>40</td> <td>6.5</td> <td>45</td> <td>381</td> <td>3</td>	10	56	25	900	40	6.5	45	381	3
13 68 10 1200 60 9 30 422 3.3 14 68 10 1200 20 9 60 502 3.8 15 43 40 1200 20 9 60 296 2.2 16 68 40 600 20 4 30 363 3.3 17 68 40 1200 60 9 60 526 4.3 18 43 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 1200 20 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 </td <td>11</td> <td></td> <td>40</td> <td>600</td> <td>60</td> <td>4</td> <td>60</td> <td>519</td> <td>3.9</td>	11		40	600	60	4	60	519	3.9
14 68 10 1200 20 9 60 502 3.8 15 43 40 1200 20 9 60 296 2.2 16 68 40 600 20 4 30 363 3.3 17 68 40 1200 60 9 60 526 4.3 18 43 10 1200 60 9 60 310 2.6 19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 1200 20 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 534 377 2.9	12	68	10	1200	20	4	30	452	3
15 43 40 1200 20 9 60 296 2.2 16 68 40 600 20 4 30 363 3.3 17 68 40 1200 60 9 60 526 4.3 18 43 10 1200 60 9 60 310 2.6 19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 600 60 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 24 56 25 900 40 6.5 45 395 2.9 25 56 25 900 40 6.5 45 395 2.9 26<	13	68	10	1200	60	9	30	422	3.3
16 68 40 600 20 4 30 363 3.3 17 68 40 1200 60 9 60 526 4.3 18 43 10 1200 60 9 60 310 2.6 19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 600 60 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 27<	14	68	10	1200	20	9	60	502	3.8
17 68 40 1200 60 9 60 526 4.3 18 43 10 1200 60 9 60 310 2.6 19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 600 60 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 30 340 1.6 27<	15	43	40	1200	20	9	60	296	2.2
18 43 10 1200 60 9 60 310 2.6 19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 600 60 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 30 340 1.6 28 68 40 600 20 9 30 340 1.6 28 68 40 600 20 9 30 430 2.9	16	68	40	600	20	4	30	363	3.3
19 68 10 1200 60 4 60 395 2.8 20 56 25 900 40 6.5 45 357 2.3 21 68 40 600 60 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 30 340 1.6 28 68 40 600 20 9 30 430 1.6 28 68 40 600 20 9 30 430 1.8 31 <td>17</td> <td>68</td> <td>40</td> <td>1200</td> <td>60</td> <td>9</td> <td>60</td> <td>526</td> <td>4.3</td>	17	68	40	1200	60	9	60	526	4.3
20 56 25 900 40 6.5 45 357 2.3 21 68 40 600 60 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31	18	43	10	1200	60	9	60	310	2.6
21 68 40 600 60 9 30 534 4 22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32	19	68	10	1200	60	4	60	395	2.8
22 56 25 900 40 6.5 45 368 2.9 23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 395 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 9 30 430 1.6 28 68 40 600 20 9 30 430 1.6 28 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31	20	56	25	900	40	6.5	45	357	2.3
23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 9 30 340 1.6 28 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 445 3.1 34	21	68	40	600	60	9	30	534	4
23 68 40 1200 20 9 30 553 3.5 24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 9 30 340 1.6 28 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 445 3.1 34	22	56	25		40	6.5	45		2.9
24 56 25 900 40 6.5 45 377 2.9 25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 4 60 335 3.4 29 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35	23		40		20	9	30		3.5
25 56 25 900 40 6.5 45 395 2.9 26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 144 3.1 34 43 10 1200 20 4 60 174 2.5 35	_					_			
26 43 10 600 20 9 60 402 2 27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 1200 60 9 30 487 2.5 38	_								
27 43 10 1200 20 9 30 340 1.6 28 68 40 600 20 4 60 335 3.4 29 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 1200 60 9 30 487 2.5 38	_								
28 68 40 600 20 4 60 335 3.4 29 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 1200 60 9 30 487 2.5 38 68 40 1200 60 4 30 344 2.5 39						_			
29 68 40 600 20 9 30 430 2.9 30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 1200 20 4 60 466 2.7 40	_								
30 43 10 600 60 9 30 449 1.8 31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 1200 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	-								
31 43 10 600 60 9 60 377 3.4 32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 1200 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	_								
32 43 10 600 60 4 60 328 2.2 33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 1200 60 9 30 487 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42<	_								
33 68 40 1200 60 4 60 445 3.1 34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 600 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 40 6.5 45 659 2.1 43	_								
34 43 10 1200 20 4 60 174 2.5 35 56 25 900 40 6.5 45 356 2.9 36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 600 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 40 6.5 45 659 2.1 43 56 25 1500 40 6.5 45 355 2.2	_								
35 56 25 900 40 6.5 45 356 2.9 36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 600 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 40 6.5 45 659 2.1 43 56 25 900 40 6.5 45 355 2.2 44 56 55 900 40 6.5 45 355 2.2	-								
36 68 40 600 20 9 60 363 3.4 37 68 40 1200 60 9 30 487 2.5 38 68 40 600 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 0 6.5 45 659 2.1 43 56 25 900 40 6.5 45 659 2.1 43 56 25 900 40 6.5 45 355 2.2 44 56 55 900 40 6.5 45 355 2.2 4	_								
37 68 40 1200 60 9 30 487 2.5 38 68 40 600 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 40 6.5 45 659 2.1 43 56 25 1500 40 6.5 45 659 2.1 43 56 25 900 40 6.5 45 355 2.2 44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 6.5 45 369 2.1 <	_								
38 68 40 600 60 4 30 344 2.5 39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 0 6.5 45 659 2.1 43 56 25 1500 40 6.5 45 273 2.2 44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 6.5 45 355 2.2 46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 <	-								
39 68 40 1200 20 4 60 466 2.7 40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 0 6.5 45 659 2.1 43 56 25 1500 40 6.5 45 273 2.2 44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 6.5 45 369 2.1 46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 387 2.0	_					_			
40 68 40 1200 60 4 30 444 2.4 41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 0 6.5 45 659 2.1 43 56 25 1500 40 6.5 45 273 2.2 44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 369 2.1 48 81 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1	_								
41 56 25 900 40 6.5 15 577 0.7 42 56 25 900 0 6.5 45 659 2.1 43 56 25 1500 40 6.5 45 273 2.2 44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 1.5 45 236 2.2 46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 387 2.0 50 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1	-								
42 56 25 900 0 6.5 45 659 2.1 43 56 25 1500 40 6.5 45 273 2.2 44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 1.5 45 236 2.2 46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 387 2.0 49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2									
43 56 25 1500 40 6.5 45 273 2.2 44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 1.5 45 236 2.2 46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 738 4.9 49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9	_								
44 56 55 900 40 6.5 45 355 2.2 45 56 25 900 40 1.5 45 236 2.2 46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 738 4.9 49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	-								
45 56 25 900 40 1.5 45 236 2.2 46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 738 4.9 49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	_								
46 56 25 900 40 6.5 45 369 2.1 47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 738 4.9 49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	44		55	900	40	6.5	45	355	2.2
47 31 25 900 40 6.5 45 140 1.7 48 81 25 900 40 6.5 45 738 4.9 49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	_				_				
48 81 25 900 40 6.5 45 738 4.9 49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	46			900	40	6.5		369	
49 56 25 900 40 6.5 45 387 2.0 50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	47	31	25	900	40	6.5	45	140	1.7
50 56 25 900 80 6.5 45 343 2.1 51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	48	81	25	900	40	6.5	45	738	4.9
51 56 25 900 40 6.5 75 302 3.2 52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	49	56	25	900	40	6.5	45		2.0
52 56 25 300 40 6.5 45 561 1.9 53 56 25 900 40 11.5 45 498 1.8	50	56	25	900	80	6.5	45	343	2.1
53 56 25 900 40 11.5 45 498 1.8	51	56	25	900	40	6.5	75	302	3.2
53 56 25 900 40 11.5 45 498 1.8	52	56	25	300	40	6.5	45	561	1.9
54 56 -5 900 40 6.5 45 286 1.6	53	56	25	900	40	11.5	45	498	
	54	56	-5	900	40	6.5	45	286	1.6

TABLE 3: HT 100-Factors and levels for 2^{nd} set of

readings

SL	Gri+	Grit Environ Rotational		Hono Eluid		Honing R _a		Power	
ЭL	Size		Speed	Hone Fluid Angle Pressure		_	na (nm)	/TT \	
	(μm)	Temp.	(RPM)	(Deg.)		(Sec.)	,,	(1111)	
		(°C)							
1	43	40	600	60	9	60	340	1.8	
2	68	10	600	20	4	60	465	3.6	
3	68	10	600	20	9	30	524	3.7	
4	43	10	1200	60	4	30	290	1.5	
5	68	10	600	60	4	30	421	2.9	
6	43	10	600	20	4	30	458	1.7	
7	43	40	1200	20	4	30	308	2.2	
8	56	25	900	40	6.5	45	383	3.1	
9	56	25	900	40	6.5	45	373	3.1	
10	56	25	900	40	6.5	45	385	3	
11	68	40	600	60	4	60	517	3.9	
12	68	10	1200	20	4	30	458	3.2	
13	68	10	1200	60	9	30	420	3.3	
14	68	10	1200	20	9	60	507	3.5	
15	43	40	1200	20	9	60	294	2.2	
16	68	40	600	20	4	30	370	3.3	
17	68	40	1200	60	9	60	535	4.3	
18	43	10	1200	60	9	60	313	2.6	
19	68	10	1200	60	4	60	398	2.8	
20	56	25	900	40	6.5	45	358	2.3	
21	68	40	600	60	9	30	539	4.1	
22	56	25	900	40	6.5	45	367	2.9	
23	68	40	1200	20	9	30	555	3.5	
24	56	25	900	40	6.5	45	378	2.9	
25	56	25	900	40	6.5	45	390	2.9	
26	43	10	600	20	9	60	405	2.2	
27	43	10	1200	20	9	30	342	1.6	
28	68	40	600	20	4	60	337	3.4	
29	68	40	600	20	9	30	434	2.9	
30	43	10	600	60	9	30	443	1.8	
31	43	10	600	60	9	60	370	3.4	
32	43	10	600	60	4	60	327	2.2	
33	68	40	1200	60	4	60	448	3.1	
34	43	10	1200	20	4	60	171	2.5	
35	56	25	900	40	6.5	45	353	2.9	
36	68	40	600	20	9	60	365	3.4	
37	68	40	1200	60	9	30	482	2.5	
38	68	40	600	60	4	30	348	2.5	
39	68	40	1200	20	4	60	460	2.7	
40	68	40	1200	60	4	30	447	2.4	
41	56	25	900	40	6.5	15	580	0.7	
42	56	25	900	0	6.5	45	658	2	
43	56	25	1500	40	6.5	45	279	2.2	
44	56	55	900	40	6.5	45	351	2.1	
45	56	25	900	40	1.5	45	237	2	
46	56	25	900	40	6.5	45	363	2.1	
47	31	25	900	40	6.5	45	144	1.7	
48	81	25	900	40	6.5	45	732	4.9	
40 49	56	25	900	40	6.5	45	381	2	
49 50	56	25	900		6.5	45	341	2.1	
50 51	56	25	900	80 40	6.5	75	306	3.2	
_									
52	56	25	300	40	6.5	45	569	1.9	
53	56	25	900	40	11.5	45	492	1.8	
54	56	-5	900	40	6.5	45	284	1.4	

TABLE 4: HT 100-Factors and levels for 3rd set of readings

SL	Grit	Environ Rotational		Hone Fluid		Honing	Ra	Power
	Size	mental Speed		Angle	ngle Pressure		(nm)	(Kw)
	(µm)	Temp (°C)	(RPM)	(Deg.)		(Sec.)		
1	43	40	600	60	9	60	334	1.7
2	68	10	600	20	4	60	469	3.6
3	68	10	600	20	9	30	522	3.7
4	43	10	1200	60	4	30	295	1.5
5	68	10	600	60	4	30	422	2.7
6	43	10	600	20	4	30	458	1.7
7	43	40	1200	20	4	30	300	2.2
8	56	25	900	40	6.5	45	384	3.1
9	56	25	900	40	6.5	45	382	3.1
10	56	25	900	40	6.5	45	384	3.1
11	68	40	600	60	4	60	519	3.9
12	68	10	1200	20	4	30	454	3.0
13	68	10	1200	60	9	30	429	3.3
14	68	10	1200	20	9	60	503	3.8
15	43	40	1200	20	9	60	285	2.2
16	68	40	600	20	4	30	377	3.3
17	68	40	1200	60	9	60	534	4.3
18	43	10	1200	60	9	60	317	2.6
19	68	10	1200	60	4	60	406	2.8
20	56	25	900	40	6.5	45	352	2.3
21	68	40	600	60	9	30	534	4
22	56	25	900	40	6.5	45	366	2.9
23	68	40	1200	20	9	30	561	3.5
24	56	25	900	40	6.5	45	386	2.9
25	56	25	900	40	6.5	45	412	2.9
26	43	10	600	20	9	60	411	2.2
27	43	10	1200	20	9	30	341	1.6
28	68	40	600	20	4	60	338	3.4
29	68	40	600	20	9	30	430	2.8
30	43	10	600	60	9	30	435	1.8
31	43	10	600	60	9	60	374	3.4
32	43	10	600	60	4	60	325	2.2
33	68	40	1200	60	4	60	453	3.1
34	43	10	1200	20	4	60	177	2.5
35	56	25	900	40	6.5	45	350	2.9
36	68	40	600	20	9	60	362	3.4
37		40	1200	60	9	30	488	2.5
38	68	40	600	60	4	30	340	2.5
39	68	40	1200	20	4	60	471	2.7
40	68	40	1200	60	4	30	452	2.4
41	56	25	900	40	6.5	15	574	0.6
42	56	25	900	0	6.5	45	653	2
43	56	25	1500	40	6.5	45	271	2.2
_		55 55			6.5	45		
44	56		900	40			347	2.1
45 46	56	25	900	40	1.5	45 4E	232	2
<u> </u>	56	25	900	40	6.5	45 4E	356	2.1
47	31	25	900	40	6.5	45 4E	138	1.7
48	81	25	900	40	6.5	45	721	4.9
49	56	25	900	40	6.5	45	380	2
50	56	25	900	80	6.5	45	335	2.1
51	56	25	900	40	6.5	75	295	3.2
52	56	25	300	40	6.5	45	561	1.9
53	56	25	900	40	11.5	45	488	1.8
54	56	-5	900	40	6.5	45	288	1.6

R.S.M. Model Construction

TABLE 5: Prediction spreadsheet with corresponding power consumptions in HT 100

SL		Model 1			Model 2			Model 3	
	R _a (Obs.)	R _a (Pred.)	(Watt)	R _a (Obs.)	R _a (Pred.)	(Watt)	R _a (Obs.)	R _a (Pred.)	(Watt)
1	325	323.237513	1.8	340	332.93884	1.8	334	323.082459	1.7
2	456	464.605161	3.6	465	468.447968	3.6	469	470.364828	3.6
3	529	539.355161	3.7	524	533.947968	3.7	522	530.114828	3.7
4	276	174.335751	1.5	290	277.554547	1.5	295	262.40645	1.5
5	433	466.029566	2.9	421	456.680715	2.9	422	453.117676	2.7
6	446	450.017569	1.7	458	460.986366	1.7	458	460.679177	1.7
7	303	323.881757	2.2	308	324.812921	2.2	300	317.67982	2.2
8	388	388.651493	3.1	383	390.080148	3.1	384	388.805298	3.1
9	370	388.651493	3.1	373	390.080148	3.1	382	388.805298	3.1
10	381	388.651493	3	385	390.080148	3	384	388.805298	3.1
11	519	439.281471	3.9	517	472.074298	3.9	519	485.581661	3.9
12	452	474.644243	3	458	481.874081	3.2	454	482.59736	3.0
13	422	430.605161	3.3	420	423.447968	3.3	429	430.364828	3.3
14	502	503.574709	3.8	507	507.350331	3.5	503	501.161387	3.8
15	296	264.545143	2.2	294	258.669616	2.2	285	252.043711	2.2
16	363	415.010482	3.3	370	420.743994	3.3	377	422.923265	3.3
17	526	548.008047	4.3	535	554.007057	4.3	534	553.378833	4.3
18	310	275.351376	2.6	313	257.228611	2.6	317	300.695905	2.6
19	395	405.355161	2.8	398	407.947968	2.8	406	414.114828	2.8
20	357	388.651493	2.3	358	390.080148	2.3	352	388.805298	2.3
21	534	500.12238	4	539	498.483388	4.1	534	493.240752	4
22	368	388.651493	2.9	367	390.080148	2.9	366	388.805298	2.9
23	553	571.237058	3.5	555	568.176754	3.5	561	569.720437	3.5
24	377	388.651493	2.9	378	390.080148	2.9	386	388.805298	2.9
25	395	388.651493	2.9	390	390.080148	2.9	412	388.805298	2.9
26	402	396.033194	2	405	396.160429	2.2	411	400.968632	2.2
27	340	405.054197	1.6	342	406.131967	1.6	341	353.702258	1.6
28	335	368.659496	3.4	337	369.689521	3.4	338	374.57065	3.4
29	430	483.500405	2.9	434	486.098612	2.9	430	415.770259	2.8
30	449	467.746567	1.8	443	460.901191	1.8	435	459.241006	1.8
31	377	408.2658	3.4	370	403.967319	3.4	374	405.284045	3.4
32	328	292.814748	2.2	327	290.58301	2.2	325	292.672824	2.2
33	445	443.818587	3.1	448	443.598612	3.1	453	448.184286	3.1
34	174	171.622378	2.5	171	171.813785	2.5	177	174.634076	2.5
35	356	388.651493	2.9	353	390.080148	2.9	350	388.805298	2.9
36	363	313.401044	3.4	365	462.847966	3.4	362	337.984803	3.4
37	487	509.159496	2.5	482	510.007703	2.5	488	515.343377	2.5
38	344	318.120104	2.5	348	414.892498	2.5	340	307.679091	2.5
39	466	451.896149	2.7	460	444.767663	2.7	471	448.561346	2.7
40	444	425.419573	2.4	447	427.403085	2.4	452	433.286901	2.4
41	577	539.06865	0.7	580	523.067457	0.7	574	606.358231	0.6
42	659	612.450252	2.1	658	589.379365	2	653	638.142804	2
43	273	329.813888	2.2	279	331.243001	2.2	271	257.311741	2.2
44	355	361.440076	2.2	351	365.533072	2.1	347	360.544488	2.1
45	236	297.932287	2.2	237	301.20382	2	232	258.778133	2
46	369	388.651493	2.1	363	390.080148	2.1	356	388.805298	2.1
47	140	205.115284	1.7	144	210.265035	1.7	138	163.58098	1.7
48	738	703.187702	4.9	732	664.89526	4.9	721	688.029615	4.9
49	387	388.651493	2.0	381	390.080148	2	380	388.805298	2
50	343	354.852734	2.1	341	355.78093	2.1	335	353.467791	2.1
51	302	332.234336	3.2	306	332.092838	3.2	295	331.968826	3.2
52	561	511.489098	1.9	569	448.917294	1.9	561	542.922336	1.9
53	498	479.370699	1.8	492	478.956475	1.8	488	475.832463	1.8
54	286	305.86291	1.6	284	414.627223	1.4	288	264.933893	1.6

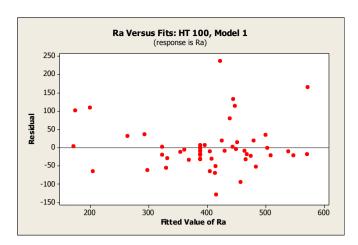


Fig. 2: Ra versus Fits plot: HT 100- Model 1

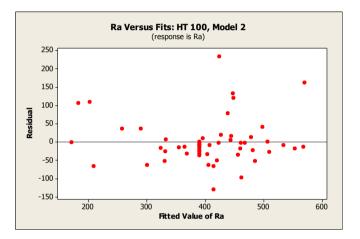


Fig. 3: Ra versus Fits plot: HT 100- Model 2

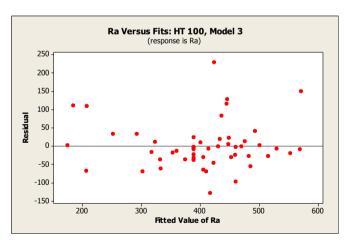


Fig. 4: Ra versus Fits plot: HT 100- Model 3

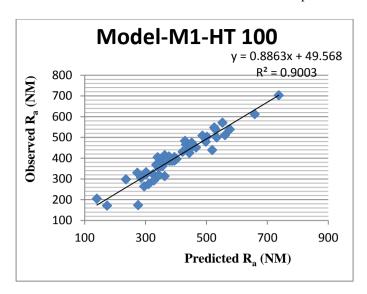


Fig. 5: Predictions against Observations of R_a for Model-M1-HT 100

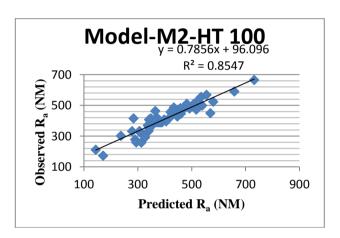


Fig. 6: Predictions against Observations of R_a for Model-M2-HT 100

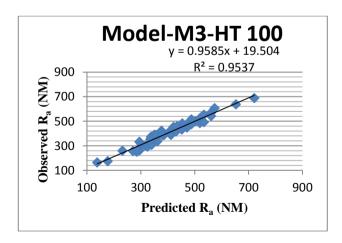


Fig. 7: Predictions against Observations of R_a for Model-M3-HT 100

Fig.2 to 4 shows the graphical representation of R_a versus fits which implicates the goodness between observed and

predicted response. The R^2 values and the slope of predictions R_a (component of surface roughness) has been represented by Fig.5 to Fig.7 The correlation coefficients of the model 1, model 2 & model 3are 0.9003, 0.8547 and 0.9537 respectively. It shows a good relationship between the two values. Its gradients are also 0.8863, 0.7856and 0.9585 which are close to unity.

Modeling Result

The following table referred to correlation coefficient between the observed and predicted values of surface roughness and root mean square error. It is very clear that higher the correlation coefficient and lower the root mean square error leads to best models. The third models of HT 100 have been selected.

Table 6: Summary of R²values of RSM modeled data

Material	Model	R² Value	Equation	Average Prediction		Percentage RMSE	Average %
				R _a (NM)	Square Error	(%)	RMSE
				(INIVI)	(Mg/Min)		
HT 100	M1	0.9003	y = 0.8863x +	406.37	34.65	8.52	8.246
			49.568				
	M2	0.8547	y = 0.7856x +	413.16	43.17	10.44	
			96.096				
	М3	0.9537	y = 0.9585x + 19.504	405.94	23.47	5.78	

Conclusion for Modelling:

The foregoing study shows that it is possible to construct reliable RSM models for surface roughness parameter of the honing process applied to the cylinder liner of a motorbike. The chief features of the model are as follows:

- (i) The central composite design of experiment is more robust than other existing modeling techniques used in honing which has already been discussed in literature review.
- (ii) It is the most compatible approach for the modeling of honing operation using very small experimental effort.
- (iii) It is the most compatible approach for the modeling of honing operation using very small experimental effort
- (iv) It is the most compatible approach for the modeling of honing operation using very small experimental effort.
- (v) MINITAB 17 has been used for the prediction of surface roughness of the cylinder liner by incorporating the all process parameters in to it.

Based on the correlation coefficient and root mean square error approach, the best models were selected as third models of HT 100.

References:

[1] Abouelatta, O.B. and Mald, J. (2001), "Surface roughness prediction based on cutting parameters

- and tool vibrations in turning operations," Journal of Materials Processing Technology, vol.118, pp269-277.
- [2] Armergo, E.J.A. and Brown, R.H. (1969), The machining of metals, Prentice-Hall Inc., Englewood Cliffs, New Jersey, pp370.
- [3] Arora, P.K. (2008), "Statistical modelling of surface roughness in turning process," M.Tech. Dissertation, Department of Mechanical Engineering, CITM, MD University, Rohtak, Haryana, India.
- [4] ASME, (1996), "Surface Texture (Surface roughness, Waviness, and Lay): An American Standard," ASME B46.1-1995 (Revision of ANSI/ASME B46.1-1985), and ASME Press, New York.
- [5] Baek, D.K, Ko, T.J., and Kim, H.S. (2001), "Optimization of feed rate in a face milling operation using a surface roughness model," International Journal of Machine Tools and Manufacture, vol.41, pp451-462.
- [6] Bernados, P.G. and Vosniako, G.C. (2002), "Predicting surface roughness in CNC face milling using neural networks and Taguchi's design of experiments," Robotics and Computer Integrated Manufacturing, vol.18, pp343-354.
- [7] Bhattacharya, A., Faria-Gonzalez, R. and Ham, I. (1970), "Regression analysis for predicting surface finish and its application in the determination of optimum machining conditions," ASME Journal of Engineering for Industry, vol.4, pp711-714.
- [8] Boothryod, G. and Knight, W.A. (1989), Fundamentals of machining and machine tools, 2nd edition, New York: Marcel Dekker.
- [9] Box, G.E.P, Hunter, W.G., and Hunter, J.S. (1978), "Statistics for experimenter: An Introduction to design, data analysis, and model building," New York, John Wiley and Sons.
- [10] Chavan P.S. et al (2013), "Effect Of Honing Process Parameters On Surface Quality Of Engine Cylinder Liners" International Journal of Engineering Research & Technology, vol 2, No 4, ISSN 2278-0181, pp 98-107
- [11] Das, S.R et al (2014), "Surface Roughness, Machining Force and FlankWear in Turning of Hardened AISI 4340 Steel with Coated Carbide Insert: Cutting Parameters Effects" International Journal of Automotive Engineering, vol 4, No 3, pp 758-768

Authors



Mr. B. N. Tripathi

Research Scolar, ISM/IIT Dhanbad Teaching & Research Experience - 13 years Research Publications - More than 05



Dr. N. K. Singh

Associate Professor, ISM/IIT Dhanbad Teaching & Research Experience - 28 years Research Publications - More than 30.