

Numerical Solutions of the Boundary-Layer Axisymmetric Flow over a Nonlinear Stretching Sheet by Spline Collocation Method

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Abstract

We study numerically the boundary-layer flow of a viscous fluid over a nonlinear axisymmetric stretchingsheet. With the help of similarity transformation, the governing partial differential equations are reduced to an ordinary differential equation. The resulting ordinary differential equation is solved using Quartic spline collocation method. The numerical solutions are obtained in the form of velocity profiles and skin friction for various values of parameters.

Keywords: Boundary- layer axisymmetric flow, stretching sheet, spline collocation, Quartic spline.

INTRODUCTION

The analysis of boundary-layer flow induced by a moving rigid surface due to Sakiadis [26] is well known. Such boundary-layer behavior over a moving continuous surface is an important type of flow that occurs in several engineering process. For example, materials manufactured by extrusion processes and heat-treated material traveling between a feed roll and a wind-up roll or on a conveyer belt possess the characteristics of a moving continuous surface. Crane [12] extended the analysis to flow induced by a stretching sheet. This problem has later been extensively studied in various directions including Newtonian and non-Newtonian fluids, porous and nonporous space and hydrodynamic and magnetohydrodynamic (MHD) fluids. Some interesting recent investigations is mentioned in the references [5–9].

In all the aforementioned studies the flow is induced by a linear stretching sheet. In spite of the growing literature on flow over stretching sheets and its obvious importance in the polymer and electrochemical industries, it is surprising to note that the corresponding analysis of nonlinear stretching sheet does not seem to have received any adequate attention so far. Recently, Vajravelu [27] discussed the boundary-layer flow of a viscous fluid over a planar nonlinearly stretching sheet. He obtained the numerical solution of the problem.

Here we analyze axisymmetric flow over a nonlinear stretching sheet numerically. By using the similarity transformation [10], the partial differential equation governing the flow are transformed to ordinary differential equation, which is solved numerically by using Quartic spline collocation method. The solutions are obtained in the form of

stream function f , velocity profile f' and skin friction $f''(0)$, for different values of parameter involved.

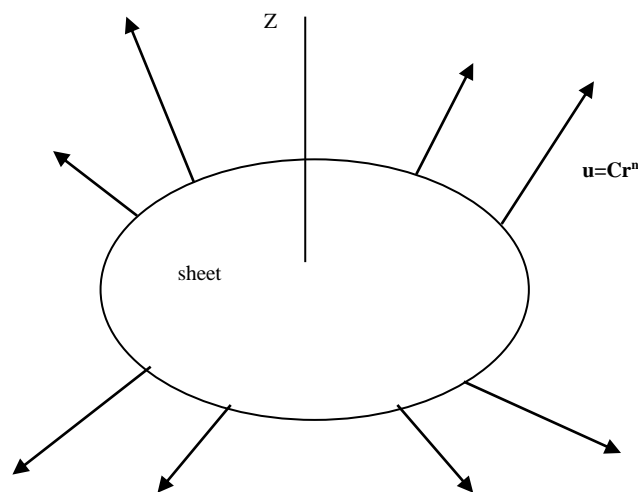


Figure 1. Geometry of the problem

MATHEMATICAL FORMULATION:

Consider the steady, laminar flow of a viscous fluid over a nonlinearly stretching sheet. The sheet is in the plane $z = 0$ and the fluid occupies the half space $z > 0$. For the mathematical modeling we take the cylindrical polar coordinate system (r, θ, z) when flow occurs under the rotational symmetry. Thus all physical quantities are independent of θ and the azimuthal component of velocity v vanishes identically. The schematic diagram of the considered geometry is given in Fig. 1.

The equations which govern the axisymmetric flow of a viscous fluid are the full Navier–Stokes equations and are given by

$$\frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial w}{\partial z} = 0 \quad (1)$$

$$u \frac{\partial u}{\partial r} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial r} + \nu \left(\frac{\partial^2 u}{\partial r^2} + \frac{\partial^2 u}{\partial z^2} + \frac{1}{r} \frac{\partial u}{\partial r} - \frac{u}{r^2} \right) \quad (2)$$

$$u \frac{\partial w}{\partial r} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial z} + \nu \left(\frac{\partial^2 w}{\partial r^2} + \frac{\partial^2 w}{\partial z^2} + \frac{1}{r} \frac{\partial w}{\partial r} \right) \quad (3)$$

where $\nu = \mu/\rho$ is the kinematic viscosity, ρ is the density, p is the pressure, and u and w are the velocities in the r and z directions, respectively. Since the flow is caused only due to the stretching of the sheet therefore the pressure gradient can be neglected. By applying the usual boundary-layer

approximations, the equations which govern the boundary-layer axisymmetric flow of a viscous fluid are Eq. 1 and

$$u \frac{\partial u}{\partial r} + w \frac{\partial u}{\partial z} = v \frac{\partial^2 u}{\partial z^2} \quad (4)$$

The boundary conditions are

$$u = ar^n, w=0 \text{ at } z = 0, \quad u \rightarrow 0 \text{ as } z \rightarrow \infty. \quad (5)$$

in which $a > 0$ is the stretching constant and n is a positive integer. Introducing the following similarity transformations

$$\eta = \sqrt{\frac{a(n+1)}{2v}} r^{\frac{n-1}{2}} z u = ar^n f'(\eta), \quad \omega = -ar^{\frac{n-1}{2}} \sqrt{\frac{2v}{a(n+1)}} \left[\frac{3n+1}{2} f(\eta) + \frac{n-1}{2} \eta f'(\eta) \right] \quad (6)$$

Eq. 1 is identically satisfied and Eq. 4 and conditions 5 gives the following equations.

$$f''' + \left(\frac{3n+1}{n+1}\right) f f'' - \left(\frac{2n}{n+1}\right) f'^2 = 0 \quad (7)$$

$$f = 0, f' = 1 \text{ at } \eta = 0 \quad (8)$$

$$f' \rightarrow 0 \text{ as } \eta \rightarrow \infty$$

The physical quantity of interest is the skin friction coefficient C_f which is defined as

$$C_f = \frac{\tau_w}{\rho(ar^n)^2} \quad (9)$$

where τ_w is the shear stress at the wall and is given by

$$\tau_w = \mu \left. \frac{\partial u}{\partial z} \right|_{z=0} \quad (10)$$

Using Eq. 6, we get

$$Re_{r^{\frac{1}{2}}} C_f = f''(0), \quad (11)$$

where $Re_{r^{\frac{1}{2}}} = 2ar^{n+1}/(n+1)v$ is the local Reynolds number. Note that for $n = 1$ one obtains the case of the linear stretching sheet

QUARTIC SPLINE COLLOCATIO :

In this section, fourth-degree spline collocation is used to construct numerical solutions to boundary value problems discussed in equation (7). A detailed description of spline functions generated by subdivision can be found in [17]

Consider equally spaced knots of a partition $\pi: a = \eta_0 < \eta_1 < \dots < \eta_n = b$ on $[a, b]$. Let $S_4[\pi]$ be the space of continuously differentiable, piecewise, Quartic polynomials on π . That is, $S_4[\pi]$ is the space of Quartic polynomials on π . The Quartic splines is given by

$$S(\eta) = a_0 + b_0(\eta - \eta_0) + \frac{1}{2}c_0(\eta - \eta_0)^2 + \frac{1}{6}d_0(\eta - \eta_0)^3 + \frac{1}{24} \sum_{k=0}^{n-1} e_k (\eta - \eta_k)_+^4 \quad (12)$$

Where the power function $(\eta - \eta_k)_+$ defined as

$$(\eta - \eta_k)_+ = \begin{cases} \eta - \eta_k & \text{if } \eta > \eta_k \\ 0 & \text{if } \eta \leq \eta_k \end{cases}$$

Consider a third order linear BVP of the form

$$u'''(\eta) + p(\eta)u''(\eta) + q(\eta)u'(\eta) + r(\eta)u(\eta) = t(\eta) ; a \leq \eta \leq b, \quad (13)$$

with boundary conditions $u(a) = k_1, u'(a) = k_2, u'(b) = k_3$

Where $u(\eta), p(\eta), q(\eta), r(\eta), s(\eta)$ are continuous functions defined in the interval $[a, b]$; K_1, k_2 and k_3 are finite real constants.

In this section, the spline solution of equations (13) is determined using a collocation method. Let (12) be an approximate solution of eq. (13), where $a_0, b_0, c_0, d_0, d_1, \dots, d_{n-1}$ are unknown real coefficients to be determined.

Let $\eta_0, \eta_1, \dots, \eta_n$ be $n+1$ grid points in the interval $[a, b]$, so that

$$\eta_i = a + ih, \quad i = 0, 1, \dots, n; \quad \eta_0 = a, \quad h = \frac{a-b}{n}. \quad (14)$$

It is required that approximate solution (12) satisfies the differential equation at the points $\eta = \eta_i$. Putting (12) in (13), we obtain the collocation equations as follows

$$a_0 r(\eta_i) + b_0 [q(\eta_i) + r(\eta_i)\eta_i] + c_0 \left[p(\eta_i) + q(\eta_i)\eta_i + \frac{1}{2}r(\eta_i)\eta_i^2 \right] + d_0 \left[1 + p(\eta_i)\eta_i + \frac{1}{2}q(\eta_i)\eta_i^2 + \frac{1}{6}r(\eta_i)\eta_i^3 \right] + \sum_{k=0}^{n-1} e_k \left[(\eta_i - \eta_k) + \frac{1}{2}p(\eta_i)(\eta_i - \eta_k)^2 + \frac{1}{6}q(\eta_i)(\eta_i - \eta_k)^3 + \frac{1}{24}r(\eta_i)(\eta_i - \eta_k)^4 \right] = t(\eta_i) \quad i=0, 1, 2, \dots, n \quad (15)$$

$$a_0 + b_0 a + c_0 \left(\frac{1}{2} a^2 \right) + d_0 \left(\frac{1}{6} a^3 \right) + \frac{1}{24} \sum_{k=0}^{n-1} e_k (\eta_i - \eta_k)_+^4 = k_1 \quad (16)$$

$$b_0 + c_0 a + d_0 \left(\frac{1}{2} a^2 \right) + \frac{1}{6} \sum_{k=0}^{n-1} e_k (\eta_i - \eta_k)_+^3 = k_2 \quad (17)$$

$$c_0 + d_0 \left(\frac{1}{2} b^2 \right) + \frac{1}{6} \sum_{k=0}^{n-1} e_k (\eta_i - \eta_k)_+^3 = k_3 \quad (18)$$

Using the power function $(\eta - \eta_k)_+$ in the above equations a system of $n+3$ linear equations in $n+3$ unknowns

$a_0, b_0, c_0, d_0, d_1, \dots, d_{n-1}$ is thus obtained. This system can be written in matrix-vector form as follows

$$AC = F \quad (19)$$

Where $C = [a_0, b_0, c_0, d_0, d_1, \dots, d_{n-1}]^T$

$$\text{and } F = [k_1, k_2, s(\eta_0), s(\eta_1), \dots, s(\eta_n), k_3]^T$$

where T denoting transpose.

The coefficient matrix A is an upper triangular Hessenberg matrix with a single lower subdiagonal, principal and upper diagonal having non-zero elements. Because of this nature of matrix A, the determination of the required quantities becomes simple and consume less time. The values of these constants ultimately yield the Quartic spline $S(\eta)$ in equation (12).

In case of nonlinear boundary value problem, the equations can be converted into linear form by any known method like quasilinearization [6] or Newton's linearization and hence this method can be used as iterative method. The procedure to obtain a spline approximation of u_i ($i = 0, 1, 2, \dots, j$; where j denotes the number of iteration) by an iterative method starts with fitting a curve satisfying the end conditions and this curve is designated as u_i . We obtain the successive iterations u_i 's with the help of an algorithm described as above till the desired accuracy.

QUARTIC SPLINE SOLUTION:

Now the nonlinear boundary value problem, the equations (7), (8) can be converted into linear form by quasilinearization [6] method as follows

$$f_{i+1}'''(\eta) + \left(\frac{3n+1}{n+1}\right) f_n(\eta) f_{i+1}''(\eta) - \left(\frac{4n}{n+1}\right) f_n'(\eta) f_{i+1}'(\eta) - \left(\frac{3n+1}{n+1}\right) f_n''(\eta) f_{i+1}(\eta) = -\left(\frac{2n}{n+1}\right) (f_n'(\eta))^2 + \left(\frac{3n+1}{n+1}\right) f_n(\eta) f_n''(\eta); n = 0, 1, 2, \dots, (n-1) \quad (20)$$

$$f_{i+1}(0) = 0, f_{i+1}'(0) = 1, f_{i+1}'(\infty) = 0 \quad (21)$$

For the numerical study the outer boundary is set at $\eta_\infty = 5$ and therefore the domain of the problem is restricted to $[0, 5]$ and end condition $f'(\infty) = 0$ is considered as $f'(5) = 0$. The collocation equation corresponding to the equations (20), (21) are obtained as follows

$$\left(\frac{3n+1}{n+1}\right) f_n''(\eta) a_0 + \left[-\left(\frac{4n}{n+1}\right) f_n'(\eta) + \left(\frac{3n+1}{n+1}\right) f_n''(\eta)(\eta_n - \eta_0)\right] b_0 + \left[\left(\frac{3n+1}{n+1}\right) f_n(\eta) - \left(\frac{4n}{n+1}\right) f_n'(\eta)(\eta_n - \eta_0) + \frac{1}{2}\left(\frac{3n+1}{n+1}\right) f_n''(\eta)(\eta_n - \eta_0)^2\right] c_0 + \left[1 + \left(\frac{3n+1}{n+1}\right) f_n(\eta)(\eta_n - \eta_0) - \left(\frac{2n}{n+1}\right) f_n'(\eta)(\eta_n - \eta_0)^2 + \frac{1}{6}\left(\frac{3n+1}{n+1}\right) f_n''(\eta)(\eta_n - \eta_0)^3\right] d_0 + \sum_{k=0}^{n-1} e_k \left[\eta_n - \eta_k + \frac{1}{2}\left(\frac{3n+1}{n+1}\right) f_n(\eta)(\eta_n - \eta_k)^2 - \frac{1}{6}\left(\frac{4n}{n+1}\right) f_n'(\eta)(\eta_n - \eta_k)^3 + \frac{1}{24}\left(\frac{3n+1}{n+1}\right) f_n''(\eta)(\eta_n - \eta_k)^4\right] = -\left(\frac{2n}{n+1}\right) (f_n'(\eta))^2 + \left(\frac{3n+1}{n+1}\right) f_n(\eta) f_n''(\eta); n=0, 1, 2, \dots, 9 \quad (22)$$

The conditions $f_{i+1}(0) = 0, f_{i+1}'(0) = 1, f_{i+1}'(5) = 0$ gives

$$a_0 = 0, b_0 = 1 \text{ and}$$

$$b_0 + 5c_0 + \frac{25}{2} d_0 + \frac{1}{6} \sum_{k=0}^{n-1} e_k (5 - \eta_k)^3 = 0 \quad (23)$$

To obtain the complete solution of the problem. We solve equations (22), (23) for the unknown $a_0, b_0, c_0, d_0, e_0, e_1, \dots, e_9$ to obtain approximate solution for $f(\eta), f'(\eta)$ and $f''(\eta)$ using equation (12). The results are obtained for different parameters involved in the problem and are presented in the table as well as in graph.

Table: 1 Stream function f

	n =1	n =2	n =3	n =4	n =5	n =10
f(0.0)	0	0	0	0	0	0
f(0.5)	0.3741596	0.3630976	0.3580974	0.3552388	0.3533867	0.3493248
f(1.0)	0.5679171	0.5394447	0.5269504	0.519913	0.5153949	0.5055987
f(1.5)	0.6636138	0.6220542	0.6042712	0.5943804	0.5880785	0.5745458
f(2.0)	0.7103019	0.6612198	0.6406458	0.6293181	0.6221444	0.6068561
f(2.5)	0.7335445	0.6809182	0.6592015	0.6473335	0.6398504	0.6239878
f(3.0)	0.7456315	0.6916784	0.669647	0.6576633	0.6501273	0.6342012
f(3.5)	0.7521318	0.6978053	0.6757462	0.6637736	0.6562527	0.6403773
f(4.0)	0.7554245	0.7009241	0.6788301	0.6668413	0.6593102	0.6434091
f(4.5)	0.7564549	0.7015859	0.6793114	0.6672112	0.6596038	0.6435229
f(5.0)	0.7555591	0.6999378	0.6772777	0.6649426	0.657177	0.6407321

Table 2: Velocity profile f'

	n=1	n=2	n=3	n=4	n=5	n=10
$f'(0.0)$	1	1	1	1	1	1
$f'(0.5)$	0.534498	0.4999815	0.4847027	0.4760609	0.4704989	0.4584027
$f'(1.0)$	0.2679954	0.2361435	0.2228544	0.2155638	0.2109587	0.2011821
$f'(1.5)$	0.1306968	0.1104735	0.1026412	0.0985121	0.0959686	0.0907424
$f'(2.0)$	0.0641696	0.0538553	0.0502932	0.0485363	0.0475007	0.0454969
$f'(2.5)$	0.0327618	0.0286219	0.0275075	0.0270501	0.0268172	0.0264651
$f'(3.0)$	0.0177196	0.016703	0.0166798	0.01676	0.0168429	0.0170972
$f'(3.5)$	0.0099139	0.0100774	0.0103554	0.0105511	0.0106884	0.0110109
$f'(4.0)$	0.0051438	0.0054297	0.0056241	0.0057417	0.0058185	0.0059844
$f'(4.5)$	0.0015795	0.0014825	0.0014327	0.0013975	0.0013713	0.0013029
$f'(5.0)$	0	0	0	0	0	0

Table 3: Skin friction $f''(0)$

n	$f''(0)$
1	-1.16583349
2	-1.30158215
3	-1.36492236
4	-1.40171394
5	-1.4257801
10	-1.47920937

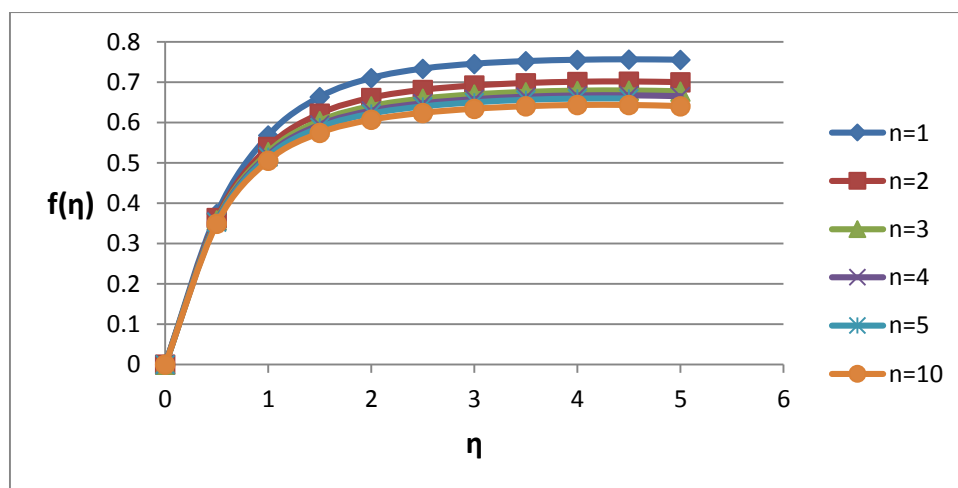


Figure 2. Variation of f with increasing of the parameter n

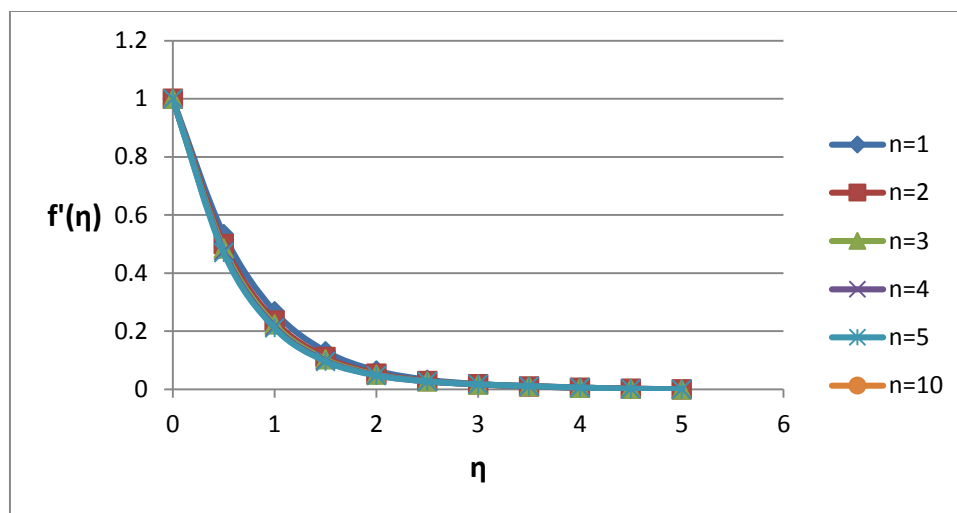


Figure 3. Variation of f' for increasing value of the parameter n

DISCUSSION OF RESULTS AND CONCLUSIONS:

The graphs of the function $f(\eta)$ and $f'(\eta)$ are drawn against η for different values of the parameter n in fig. 2 and 3. Here the parameter n is a measure of nonlinearity of the stretching sheet.

It is shown in Fig. 3 that the velocity f' and boundary-layer thickness decreases by increasing the parameter n . Fig. 2 shows that the f decreases as η increases whereas the boundary-layer thickness increases. It is also observed that the flows does not noticeably depend on n for $n \geq 15$. The values of the skin friction and fractional darg coefficient are given in Table 3. It is clear form table 3 that the magnitude of skin friction coefficient increases with an increase in n . Also the first value in table 3 for the linear stretching case ($n=1$) is exactly the same when compared with the numerical and perturbation solutions presented in [3]. This shows that the Quartic spline collocation results agree well with the numerical and analytical ones.

In this paper, analysis of the axisymmetric flow of a viscous fluid over a nonlinearly stretching sheet is carried out. The numerical solutions are presented using the Quartic spline. The effect of the parameter n on the velocity are presented graphically and discussed. It is found that the effect of the parameter n is small for $n \geq 15$. Moreover, the results of the linear stretching sheet can be derived form the presented solution for $n=1$ and are quite comparable with the existing results as presented in [3]

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