

## Investigation On Full Bridge And Coupled Inductor ZVS DC-DC Converter Fed PMDC Motor

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### Abstract

The Power converters are extensively used in medium to high power application. For most of these applications, the most desirable features of isolated converter are high efficiency, high power density, high reliability and low electromagnetic interference. A soft switching which is bidirectional DC-DC converter is proposed. Soft switching technique is used to achieve high power density, good switching frequency and improved efficiency. The switching losses proportionally increase with an increase in switching frequency, thus limiting the maximum switching frequency of the power converters. But, high switching frequencies are the best solution when low weight and size converters are needed. This paper present work, two topology of converter are designed and simulated. Looking at the social relevance aspect, this bidirectional converter behaviour is simulated with DC motor applications. Use of this experimented prototype would further improve the social relevance on the terminal users in terms of cost, size, operation, compatibility and reliability. The results are compared and the best one is identified. Hardware has implemented for the isolated and non-isolated Coupled inductor bidirectional DC-DC converter.

**Keywords:** Bidirectional DC-DC converter, Full Bridge DC-DC Converter, Coupled Inductor DC-DC Converter, Boost converter PM D.C motor.

## 1 INTRODUCTION

It is used as an energy storage device which consists of resonant inductors and diodes to recover the energy stored in the capacitors back to the supply side. Many authors have studied experimentally and numerically the operation of power converters at higher switching frequencies and power levels. They have analyzed different converter topologies to minimize the switching losses and stress of the power semiconductor devices. Some of these literature related to the present study are presented. The design procedures for selecting step down ratio transformer which do not solve the problems like the leakage inductance and parasitic capacitance which resulted in reducing efficiency [1]-[2]. The design of high frequency switching mode power supplies could be applied for high power application. This has been presently recognized and so the FB-ZVS-PWM (Full Bridge Zero Voltage Switching Pulse Width Modulation) is considered as one of the best power converters. This is because it possesses the basic desirable characteristics of both the hard switching PWM converters and the soft switching ones, while avoiding their major drawbacks, such as commutation losses in the former and variable switching frequency and high conduction losses in the second group. However, the power switches of the FB-ZVS-PWM converter are subjected to the maximum input voltage level [3-4]. The snubber, proposed by these authors, uses an auxiliary switch to discharge the snubber capacitor. Generic snubber cell is identified for all the non-isolated DC-DC converters. It was implemented a soft-switching active snubber to reduce the turn-off loss of the IGBT (Insulated Gate Bipolar Transistor) in a buck converter to reduce the switching losses [5-7]. A lossless turn on snubber and mainly used to reduce the turn-off loss. The turn-off loss depends on the size of the snubber capacitance in the converter [8]. There have been proposed that when switching frequency increases, switching losses decrease and Electro Magnetic Interference (EMI) noise increase.

These problems are solved by using soft switching techniques. The MOSFET operates at Zero Voltage Switching (ZVS) turn-off and near Zero Current Switching (ZCS) turn-on. The freewheeling diode is also commutated under ZVS. As an example, operation principles, theoretical analysis, relevant equations and experimental results of a boost converter equipped with the converter are presented in detail [9].

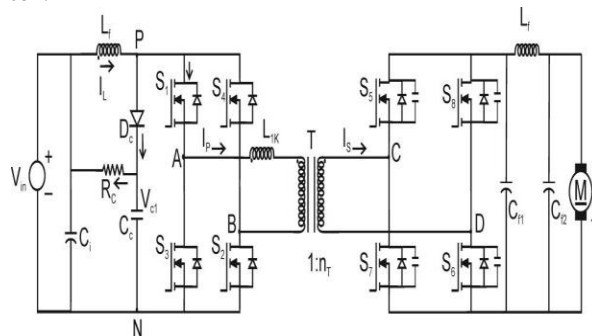
This paper was proposed a passive lossless snubber cell for non-isolated PWM DC-DC converters. A general passive loss less snubber cell for non-isolated PWM DC-DC converters was explained. The general snubber cell is the contribution of a turn-on snubber and a turn-off snubber. Energy recovery is achieved by passive components only. Component values of the snubber inductor, snubber capacitor and buffer capacitor can be determined [10]. A passive soft-switching snubber which employs a diode/capacitor snubber circuit for each switching device in an inverter to provide low  $dv/dt$  and low switching loss to the device. The circuit uses a transformer based energy regenerative circuit to recover the energy captured in the snubber capacitors [11]. It was implemented an increasing new ripple focus on the power electronic converter interface for DC energy sources. DC energy sources that have a role in distributed generation and sustainable energy systems are the photovoltaic (PV) panel, the fuel cell stack and batteries of these converters. Each half panel or

panel substring connecting into series strings avoid many of these problems. This paper examined the advantages, difficulties and implementation issues of using a cascaded converter connection for a series string of PV panels or more generally DC energy sources. A proposed residential grid connected solar installation consisting of twelve 12V, 60W, and PV panels is used [12]. In the bidirectional converter which can operate with a continuous inductor current, fixed switching frequency and switch stress of a conventional bidirectional DC-DC converter which improve the efficiency of the filter regardless of the direction of power flow [13-22].

**2. FULL BRIDGE ISOLATED BIDIRECTIONAL DC-DC CONVERTER**

It is well suitable for low input voltage and high current application. A dual full bridge topology is developed to achieve higher power rating, power density and efficiency. However switching losses have been an obstacle for high frequency operation. In general, various soft switching techniques have been used to reduce the switching losses and stress of a power device. The significant performance improvements, as well as cost, size and weight reduction could be achieved with the help of soft-switching. Fig 2.1 shows the full bridge isolated bidirectional DC-DC from low voltage side to the high voltage side, the circuit works in boost mode, to keep high voltage side at a desired high value.

In the other direction of power flow, the circuit works in buck mode to keep low voltage side at a desired low value. The output voltage is rectified and filtered to get smooth DC. Converter with  $\pi$  filter. The circuit consists of inductor in the input side and two full bridges, each are placed on each side of the main transformer. Each switching device has a small parallel capacitor for soft switching. When power flows from low voltage side to the high voltage side, the circuit works in boost mode, to keep high voltage side at a desired high value. In the other direction of power flow, the circuit works in buck mode to keep low voltage side at a desired low value of high frequency switching mode power supplies could be applied for high power application. The output voltage is rectified and filtered to get the smooth DC. The isolated bidirectional DC-DC converters are widely used in UPS battery charging and discharging systems [13-18]. This converter can be operated with constant frequency at the entire circuit. The bidirectional DC-DC converter is operated with the transformer. The proposed full isolated bidirectional DC-DC converter is compared at the load side of  $\pi$  filter.



**Fig 2.1 Isolated boost full bridge DC-DC converters**

The circuit operates bidirectional DC-DC converter as shown in Fig 2.1. Isolated boost full bridge DC-DC converter is used for medium and high power application. The work analyses the reason for the proposal PI controller and discusses the cause for the inability of performing the same operation in the open loop. This is because of the fact that the open loop is unable to maintain the constant voltage with the variations of inputs. The boost inductance  $L$  and the output filter capacitor  $C$  are calculated based on the following equations.

$$L = V_o \delta / f \Delta I \quad (2.1)$$

$$I_o = V_o / R \quad (2.2)$$

$$P_o = V_o^2 / R \quad (2.3)$$

$$E_1 = 4.44 N_1 \Phi_f f \quad (2.4)$$

$$E_2 = 4.44 N_2 \Phi_f f \quad (2.5)$$

$$C = \delta / 2 f R \quad (2.6)$$

$$V_o = V_{in} \delta \quad (2.7)$$

Where  $\delta$  = duty cycle and  $\Delta I$  = ripple current in amps. Applying Kirchoff's rule as shown in Fig 2.1 and rearranging the terms, the following results are obtained.

$$V_o = \frac{V_{in}}{(1-\delta)} \quad (2.8)$$

$$\text{Resonant impedance } Z = \sqrt{\frac{L_r}{C_s}} \quad (2.9)$$

$$\text{Resonant frequency } \omega = \frac{1}{\sqrt{L_r C_s}} \quad (2.10)$$

$$C_s = \frac{I_L t}{2V_o} \quad (2.11)$$

Therefore,

$$L = V_{in} \frac{dt_{on}}{dI} \quad (2.12)$$

$$= 5\mu\text{H}$$

Similarly, the current through the output capacitor  $C$  is,

$$I_o = C \frac{dV_o}{dt_{on}} \quad (2.13)$$

Therefore,

$$C = I_o \frac{dt_{on}}{dV_o} \quad (2.14)$$

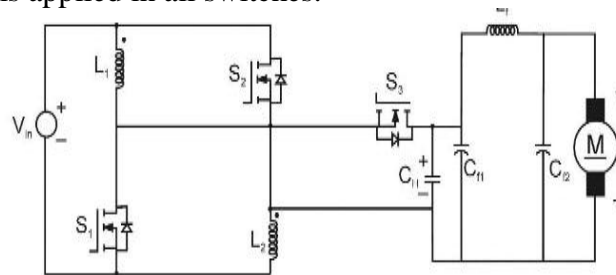
$$= 100 \mu\text{F}$$

The transfer function of a PI controller is often written in this form.

$$G_p i(s) = K_p + K_i/s \quad (2.15)$$

### 3. COUPLED INDUCTOR BASED DC-DC CONVERTER

The bidirectional DC-DC converters are widely used in UPS battery charging and discharging systems. Fig 3.1 shows the coupled inductor based bidirectional DC-DC converter. This converter employs a coupled inductor with the same winding turns in the primary and secondary sides. In step up mode, the primary and secondary windings of the coupled inductor are operated in parallel-charge and series discharge to achieve high step up voltage gain. In step down mode, the primary and secondary windings of the coupled inductor are operated in series-charge and parallel-discharge to achieve high step down voltage gain. It is used in high voltage operation. Zero voltage switching is applied in all switches.



**Eig 3.1 Coupled inductor bidirectional DC-DC converter**

$$L_1 = L_2 = L \quad (3.1)$$

$$M = k\sqrt{L_1 L_2} = kL \quad (3.2)$$

$$V_{L1} = L_1 \frac{di_{L1}}{dt} + M \frac{di_{L2}}{dt} = L \frac{di_{L1}}{dt} + kL \frac{di_{L2}}{dt} \quad (3.3)$$

$$V_{L2} = M \frac{di_{L1}}{dt} + L_2 \frac{di_{L2}}{dt} = kL \frac{di_{L1}}{dt} + L \frac{di_{L2}}{dt} \quad (3.4)$$

$$V_o = V_C = \frac{1-\delta}{1-2\delta} V_i \quad (3.5)$$

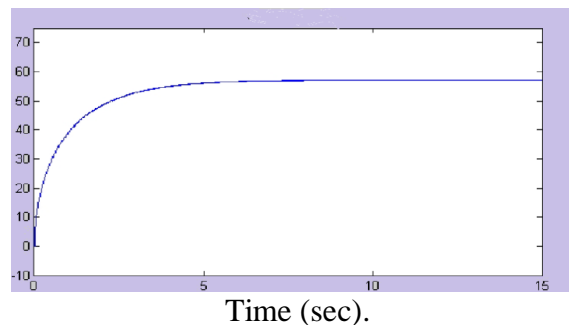
$$Z_r = \sqrt{\frac{L_{r1}}{C_{r2}}} = \sqrt{\frac{L_{r2}}{C_{r4}}} \quad (3.6)$$

$$\omega_r = \frac{1}{\sqrt{L_{r1}C_{r2}}} = \frac{1}{\sqrt{L_{r2}C_{r4}}} \quad (3.7)$$

Thus, the converter has higher step up and step down voltage gains than the conventional and full bridge bidirectional DC-DC boost/buck converter.

#### 4 SIMULATION RESULTS OF FULL BRIDGE DC-DC CONVERTER

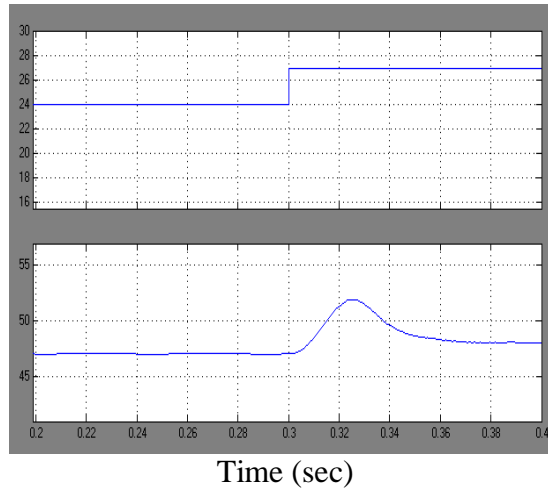
Full bridge DC-DC converter is modelled and simulated using SIMULINK version 7.9 of MATLAB and the results presented here. The output voltage of boost mode operation is 54V. It is shown in Eig4.1 It is observed the simulation of boost mode with motor load the output voltage and speed are increased in the proposed full bridge isolated DC- DC converter.



**Eig 4.1 Output voltage in boost mode**

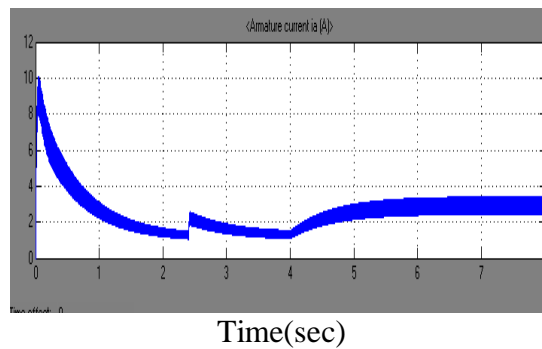
Open loop output voltage waveform with step input voltage and the output voltage waveform for closed loop controlled converter are shown in Fig 4.2 (a) and (b). Irrespective of the input voltage applied, the output voltage is maintained constant. There is a steady state error in the output of open loop system. The output

voltage is sensed and it is compared with the reference voltage. The error signal is given to the comparator through PI controller



**Fig 4.2 (a) DC output voltage with stepchange at the input (b) DC output voltage for the closed loop controlled converter operation**

This gives high output voltage and efficiency; and any further increments of input voltage will not significantly increase the ripple content. The reduction in the ripple of the proposed converter compared with the conventional one at different input voltage and load conditions, Closed loop output current is 2.5 A as shown in Eig4.3 Comparison of efficiency in boost mode is shown in table1

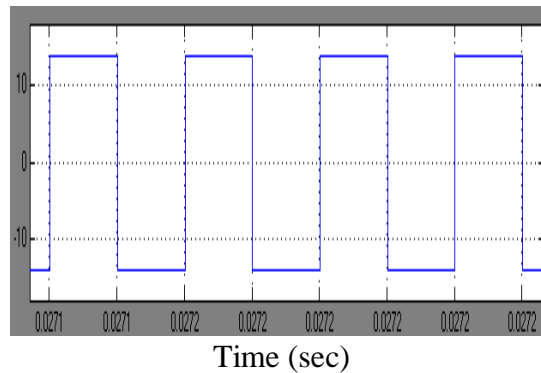
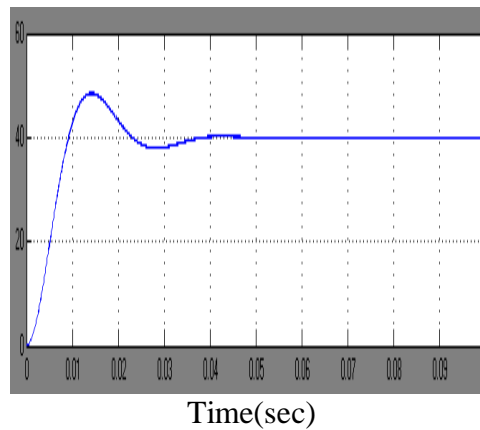


**Eig 4.3 Armature current of closed loop system**

**Table 1 Comparison of efficiency in boost mode**

Input voltage(V)	Conventional full bridge Efficiency%	Proposed full bridge Efficiency%
12	81.23	84.93
16	84.85	85.31
20	85.82	88.42
24	88.10	89.58

It is observed the simulation of boost mode with motor load the magnetizing leakage reactance is decreased than the conventional isolated full bridge DC- DC converter. Voltage across the inductor value which is 11V is shown in Eig 4.4. The boosted DC output voltage of 40V is show in Eig4.5. The DC output current of 4amp is shown in Eig 4.5. It is observed the simulation of boost mode ripple is decreased than the conventional non- isolated DC- DC converter., it is important to improve the efficiency Parameters used for simulation ( Full Bridge DC-DC Converter& Coupled inductor) are presented in the table 2 and 3 respectively

**Eig 4.4 Voltage across the inductor L<sub>2</sub>****Eig 4.5 Output voltage waveform**



Time(sec)

**Eig4.6 Output current waveform****Table 2 Parameters used for simulation (Full Bridge DC-DC Converter)**

Input Voltage	12-15V
Switching Frequency	20KHz
Pulse period	5 $\mu$ s
Capacitance	1500 $\mu$ f
Load Resistance	1000 $\Omega$
Diode	MUR150
MOSFET	IRF840
Transformer	High frequency transformer

**Table 4 Parameters used for Simulation (Coupled Inductor)**

Input Voltage	12V-15V
Switching Frequency	55KHz
Pulse period	18 $\mu$ s
InductanceL1=L2	1Mh
Capacitance	500 $\mu$ f
Load Resistance	10 $\Omega$
Diode	MUR150
MOSFET	IRF840

**Table 5 Performance of coupled inductor with Various Filters**

Filters	Parameters	Load Values (with motor)	Load Values (without motor)
C Filter	Input Voltage	12V	12V
	Output voltage	72V	74V
	THD	3.1%	3.11%
	Efficiency	91.67%	92.67%
LC Filter	Input Voltage	12V	12V
	Output voltage	45V	56V
	THD	2.3%	2.2%
	Efficiency	87.5%	88%
$\pi$ Filter	Input Voltage	12V	12V
	Output voltage	60.98	45V
	THD	2.6%	2.3%
	Efficiency	90.03%	92.95%
RC Filter	Input Voltage	12V	12V
	Output voltage	49V	64V
	THD	3.0%	3.0%
	Efficiency	82.04%	84.34%

### 5.HARDWARE RESULT OF FULL BRIDGE DC-DC CONVERTER

Transformer, it can be used to step down or step up a DC voltage source. The regulation is normally achieved by PWM at a fixed frequency. The switching device used here is n-channel enhancement MOSFET. After smoothing out the ripples, the regulated voltage is fed to the 0-24V, 2.5A, 96W, DC motor. They provide smooth acceleration control, high efficiency and fast dynamic response. A laboratory model for the isolated boost DC to DC converter is fabricated and tested. Hardware is implemented as shown in Fig 5.1. Boost mode voltage which is 45.6V is shown in Fig 5.2. Fig 5.3 shows the transformer secondary voltage which is 54.07V. Experimental results further demonstrated the feasibility of the proposed ideas. The efficiency with motor load is 90%.

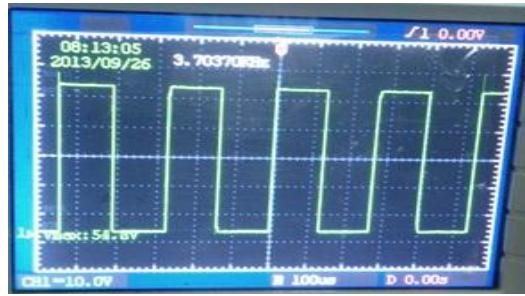


**Eig 5.1 Hardware circuit for full bridge isolated DC-DC Converter**



**Time (sec) X-axis 1unit=18μsec y-axis 1unit=20 V**

**Eig 5.2 Boost output voltage**



Time (sec) X-axis 1unit=18μsec y-axis 1unit=10V

**Eig 5.3 Transformer secondary voltage**

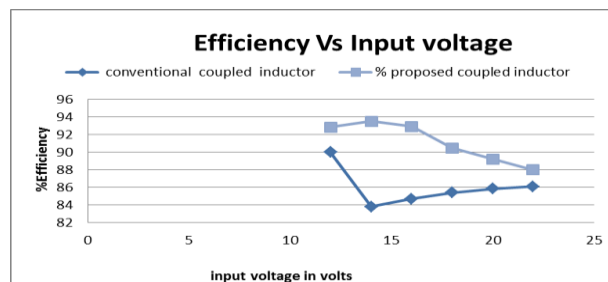
When R-load is connected to this coupled inductor bidirectional DC-DC converter, the efficiency is 92.58%. Boost mode coupled inductor output voltage is 45.6V as shown in Eig5.4



Time (sec) X-axis 1unit=18μsec y-axis 1unit=20V

**Eig 5.4 Boost mode coupled inductor output voltage**

The different values of the input voltage, the output voltage, input power, output power and hence efficiency is calculated. The values are tabulated and they are given in Table6. The different values of the input voltage and efficiency are calculated as shown in Fig 5.5.



**Fig5.5 Input voltage and %Efficiency**

**Table 6 Simulation and Experimental Result of proposed converter**

<b>Input voltage (V)</b>	<b>Output voltage (V)</b>	<b>Input power (W)</b>	<b>Output power (W)</b>	<b>Efficiency (%)</b>	<b>Mode</b>
12	28	62.23	53.33	85.98 Conventional	Simulation
12	30	60.45	54.37	89.94 Proposed	Simulation
12	54.56	30	60.45	89.94 Proposed	Full bridge hardware
12	35	60.45	54.56	90.28 Conventional	Simulation
12	40	60.97	56.67	92.94 Proposed	Simulation
12	56.67	40	60.97	92.94 Proposed	Coupled non-isolated hardware

## 6.CONCLUSION

Full bridge DC-DC converter is isolated between the two sides through a transformer. The open loop and closed loop results are presented. This circuit is capable of performing DC-DC Conversion with high efficiency. Coupled inductor DC-DC converter in open loop operation with resistive load and DC motor load. The circuit configuration of the coupled inductor DC-DC converter is superior to the full bridge DC-DC converter. It is very simple, less in size, and less in space. In this work, the performance of the coupled inductor DC-DC converter with  $\pi$  filter that produces 90% higher efficiency are compared with the other converters. The coupled inductor DC-DC converter has higher step-up and step down voltage gains and lower average value of the switch current than the conventional bidirectional boost/buck converter. The hardware and simulation results are presented From the investigation, it has been found that the proposed nonisolated coupled inductor converter has better output voltage and efficiency than that of the conventional and full bridge converter.

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