Influence of Control Surfaces in Aircraft Wing Control Reversal Problems-FEA and CFD Analysis

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Abstract

In the present work, 3-D wing with control surfaces has been taken for investigating the problems of static aero elasticity – in particular control reversal problem. To give an insight into these problems, a 2D airfoil with leading edge slat is analyzed by using GAMBIT and FLUENT. Later a 3-D swept back wing with control surfaces, designed and investigated using CFD/MSE Nastran/Patran is at the velocity of 210 m/s for 15 degree deflection if ailerons. To avoid the wing twist caused by aileron deflection, flap has been deflected in order to create a negative twist so that aileron swing can counteract by flap. This has been validated by carrying out the stress analysis of the 3-d wing. Computational analysis also carried out to investigate the effect of sweep as well as the control surfaces at the control reversal speed. This shows that to get the rolling power at the reversal speed the control surface which is located near to the root will alter the pressure distribution and hence aileron reversal can be offset.

Keywords: Control reversal-sweptback wing-low speed analysis-CFD.

1. Introduction

Fluid structure interaction will lead to physical phenomena where inertial, elastic and aerodynamic forces, acting on a structural member exposed to an airstream, have a
significant influence. Some of these phenomena are associated with high risk and can lead to structural failure. A reliable analysis of these phenomena is therefore needed to elaborate the wing design and take decisions. Aileron reversal is when the control surfaces reach an adverse effect on the controllability of the aircraft. Beyond a critical speed, called "reversal speed", an unexpected response of the aircraft appears with control surfaces deflection. Due to an insufficient torsional stiffness of the wing, the airflow may be great enough that the force generated by the ailerons twists the wing itself counteracting the intended effect of the control input. Aeroelastic interactions determine airplane loads and influence flight performance in four primary areas: Wing and tail surface lift redistribution that change external loads from preliminary loads computed on rigid surfaces; Stability derivatives, including lift effectiveness, that affects flight static and dynamic control features such as aircraft trim and dynamic response; Control effectiveness, including aileron reversal, that limits maneuverability; Aircraft structural dynamic response to atmospheric turbulence and buffeting, as well as structural stability, in particular flutter. By coupling advanced computational fluid dynamics (CFD) tools and computational structural dynamics (CSD) tools, a more accurate portrayal of the nonlineairities of the flow and the aeroelastic effects of the wing can be captured. Mostafa .S and A. Elsayed Ramin[1], Accurate Stick Model Development for Static Analysis of Complex Aircraft Wing-Box Structures AIAA 2009. This Paper investigated the process of generating a wing stick model is investigated. Ales Kratochvil in his journal [2] “Aeroelasticity analysis of wing UL-39” Journal of aircraft 2003. The computation of modal and flutter characteristic, investigating ailerons effectiveness and determines torsion divergence critical velocity at right half-wing of the aircraft UL-39. Christian Reschke and, Thiemo Kier presented the paper “An Integrated Model for Aeroelastic Simulation of large flexible Aircraft using MSC.Nastran” [3] Robotics and mechatronics, 2004. Newer computational methods can now incorporate the structural flexibility of the wing. The inclusion of flexibility allows for a better correlation between computational and experimental data [5].

2. Project Scope and Analysis
2.1 Scope:
Study of control motion of wing and static aeroelastic existing problem due to control motion. Study of structural response of aeroelastic high aspect ratio swept wing at reversal speed. Study of existence solved technique for aeroelastic instability. Computing the force exerted on aileron due dynamic pressure of air when aileron is deflected by theoretical relation. Computational design of swept wing with multiple control surfaces in high subsonic flow. Computation analysis of wing with control surface deflection when pressure force acting on aileron shaded area.
2.2 WingModelling
Aerofoil NACA 64-210; Span-60m; Sweep angle-30 Deg; Aspect ratio-8.7; Sweep at c/4 point-25.5 deg; Taper ratio-0.4; Root chord-10m; Tip chord-4m; Max. thickness of airfoil-10% of chord; Aileron location-6m from tip; Flap location-8.7m from root; Mean aerodynamic chord-7.43 m; Aileron span-7.5m; Flap span-3.3m

Fig. 1: wing model with ribs and spars, twisted wing assembly

<table>
<thead>
<tr>
<th>S. No</th>
<th>Velocity m/s</th>
<th>Displacement (mm)</th>
<th>Max Stress MPa</th>
<th>Max Strain MPa</th>
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<tr>
<td>1</td>
<td>80</td>
<td>933</td>
<td>91.24</td>
<td>1.24</td>
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<tr>
<td>2</td>
<td>90</td>
<td>1057</td>
<td>102.66</td>
<td>1.39</td>
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<tr>
<td>3</td>
<td>100</td>
<td>1175</td>
<td>114.05</td>
<td>1.55</td>
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</tbody>
</table>

Fig. 2: Deformation of wing at 90m/s at Load 2287.5N (6 flap deflection) Table.1 Values for 6 deg deflection of aileron.
Table 2: Twist variation at tip.

<table>
<thead>
<tr>
<th>S. No</th>
<th>Velocity (m/s)</th>
<th>Twist at tip due to aileron deflection (deg)</th>
<th>Twist at tip due to flap deflection (deg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>90</td>
<td>2.8</td>
<td>2.1</td>
</tr>
<tr>
<td>2</td>
<td>110</td>
<td>3.04</td>
<td>2.2</td>
</tr>
<tr>
<td>3</td>
<td>150</td>
<td>3.3</td>
<td>2.5</td>
</tr>
<tr>
<td>4</td>
<td>180</td>
<td>3.7</td>
<td>2.9</td>
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Analysis of wing with control surface is done by varying angle of attack and velocity. Boundary condition is pressure acting on aileron shaded area and span wise lift distribution on the elastic axis. Incremental lift due to aileron deflection are calculated by theoretical calculation. By having this boundary condition computation model is analyzed for 3 deg, 6 deg, 9 deg and 15 deg. At velocity 240 m/s and 15 deg deflection of aileron have Max displacement at tip is 3.078 mm. From the displacement, stress and strain plot. Max Principle stress max principle strain displacement at tip is increase with incremental of aileron deflection angle and incremental of velocity. Aileron produces torsion twist which can be counteracting by the control surface located near the wing.

3. CFD Analysis

In this study, the half-symmetric model was imported into GAMBIT as a STEP file and cleaned up using the “Heal Geometry” option during the import itself. To improve geometric connectivity and duplicate-face issues, the geometry was cleaned up and patched using ‘Clean Up Tools’.

After cleanup, a brick was created around the aircraft as a part of defining a flow volume, aligned such that the symmetry plane of the aircraft and the symmetry plane of the brick coincided and are stitched together to form a single virtual face. The brick’s high-level geometry (volume) is deleted leaving behind its low-level geometry (faces) and subsequently stitched to form a virtual flow volume.

Table 3: boundary conditions.

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<th>WALL</th>
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<tbody>
<tr>
<td>AILERON</td>
<td>WALL</td>
</tr>
<tr>
<td>FARFEILD</td>
<td>PRESSURE FAR FIELD</td>
</tr>
<tr>
<td>SYMETTRY</td>
<td>SYMMETRY</td>
</tr>
<tr>
<td>WING</td>
<td>WALL</td>
</tr>
</tbody>
</table>

If the mesh characteristics and growth are not controlled, then highly skewed elements might be formed that can adversely affect numerical computations for the resultant mesh. Hence to tackle such problems, an option called “Size Functions” that can be used to specify the rate at which volume mesh elements change in size in
proximity to a specified boundary. For this reason, two types of size functions were created and attached to control the mesh sizes in the regions adjacent to the airplane geometry surfaces.

4. Results and Discussions
Case I: comparison plots for the Ideal wing between computational and wind tunnel results.

**Fig. 6:** Comparison plot of Cl vs. alpha without any control surface deflection Figure 9.34 comparison plot of Cd vs. alpha without any control surface deflection.

**Fig. 8:** Comparison plot for Cm vs. Angle of attack, without any control surface deflection Fig9., plot of Cm vs. alpha for the aileron deflection for 3 degrees.
Fig. 10: Comparative Cl vs. alpha plots for various angle of aileron deflections.

From the above test data, it is very clear that with increase in sweep angle, there is a decrease in the lift generated and so is the case with the lift coefficient. Decrease in drag produced as well which is also apparently the same trend shown by the drag coefficient. This clearly validates the findings from the CFD analysis which have been corroborated hence. Conclude deformation at tip is high, Stress and strain near the root is high, At velocity 210m/s for 15 deg deflection of aileron have Max displacement at tip this will the adverse effect control motion if the aileron deflection will cause wing twist at tip, Tip will stall before root at that time aileron is ineffective to create the rolling power. Flap deflection created the negative twist so that aileron twist can be counteracting by flap. To get rolling power at reversal speed, we want to operate control surface which is located near the root.

References


